

TECHNICAL MEMORANDUM

DATE: September 14, 2018 **PROJECT #:** 605.8401

TO: Vicky Peacey, Resolution Copper

FROM: Chris Gregory and Tim Bayley

PROJECT: Proposed Near West Tailing Storage Facility, Resolution Copper

SUBJECT: TSF Alternative 4 – Silver King: Life of Mine and Post-Closure Seepage Transport Modeling

Introduction

The draft environmental impact statement for the proposed Resolution Copper (RC) mine includes the following tailings storage facility (TSF) alternatives:

- Alternative 2: Near West Modified Proposed Action (Modified Centerline Embankment – “Wet”)
- Alternative 3: Near West Modified Proposed Action (High-density Thickened NPAG Scavenger Tailings and Segregated PAG Pyrite Tailings Cell – “Dry”)
- Alternative 4: Silver King Filtered
- Alternative 5: Peg Leg
- Alternative 6: Skunk Camp

At the request of RC, Montgomery & Associates (M&A) has prepared this technical memorandum to document groundwater transport modeling and results for TSF Alternative 4—Silver King Filtered. The purpose of the model is to provide a tool to compare the relative impacts of seepage (rate, transit time, and quality) among the different TSF alternatives. All TSF alternatives can comply with groundwater and surface water standards, but the degree of seepage management needed among alternatives would vary (minimal/simple to extensive/complex).

The model was developed using the Contaminant Transport (CT) Module of the GoldSim simulation platform (version 12.0). The results include time series estimates of chemical constituent concentrations at Whitlow Ranch Dam and within the Queen Creek alluvial aquifer nearest to the TSF—designated “Queen Creek 3”. The model period spans

245 years, which includes the 41-year planned Life of Mine (LOM) and an additional 204 years following closure.

The GoldSim modeling provides a basis for comparison among the alternatives, but is not typically used or adequate for water quality permitting. The TSF will be required to obtain an aquifer protection permit from the Arizona Department of Environmental Quality. By regulation, every permitted facility must utilize Best Available Demonstrated Control Technology (BADCCT) and demonstrate that Aquifer Water Quality Standards (AWQS) and surface water quality standards will not be exceeded at the point of compliance as a result of discharge from the facility. These requirements have not been addressed by the GoldSim model but will be incorporated into final design, construction and operation of the TSF.

This memorandum comprises the following sections:

- Conceptual Model
- GoldSim Seepage Transport Model
- Results
- Discussion and Conclusions

Conceptual Model

Site Description

The proposed Silver King tailings alternative is located approximately 4 miles north of the town of Superior, in Pinal County, Arizona (**Figure 1**). The TSF footprint is located within the subbasins that drain into Potts Canyon, Happy Camp Canyon, and Silver King Wash. The natural land surface elevation of the proposed TSF footprint varies from approximately 2,800 to 3,800 feet above mean sea level.

Geology

A geologic map of the area showing geologic units, structures, and the proposed TSF footprint considered for Alternative 4 is shown on **Figure 2**. General descriptions of the principal hydrogeologic units (HGUs) within the Superior Basin study area were presented in the conceptual hydrogeologic model report for Near West (M&A, 2017b). Detailed characterization of the geology comprising these HGUs were described by M&A (2013 and 2017a) based on characterization studies and the work of Spencer and Richard (1995), Spencer and others (1998), Scarborough (1989), Peterson (1969), Ferguson and Trapp (2001), Ferguson and Skotnicki (1995), Richard and Spencer (1998), and Keith (1983).

Surface Water Flows

Major drainages underlying the proposed TSF footprint include Silver King Wash to the east, Potts Canyon to the west, and Happy Camp Canyon in the center. Happy Camp Canyon is divided into East and West segments in the GoldSim model. Water moves through these drainages towards the southwest, where all water not lost to groundwater evapotranspiration (GET) eventually discharges into Queen Creek. From Queen Creek, flows are redirected approximately 7 miles west to Whitlow Ranch Dam, an earthen dam that serves as the exit point for all surface water leaving the basin. Surface water flows in the canyons are infrequent and generally require large precipitation events to generate run-off.

Groundwater Flow

The direction of groundwater movement in bedrock aquifers follows the general trend of land surface topography from upland areas in the northern, eastern, and southern boundaries of the Superior Basin toward Queen Creek. The bedrock aquifers are intersected in some locations by alluvial channels with much higher hydraulic conductivities that serve as conduits for relatively rapid subsurface flow towards Whitlow Ranch Dam (M&A, 2017b). Because these alluvial channels are the primary conduits for groundwater flow to Whitlow Ranch Dam, this model only considers groundwater transport through the alluvium. Whitlow Ranch Dam is conceptualized as the ultimate exit point for all groundwater leaving the Basin; in front of the dam, groundwater is forced to land surface and exits the basin as surface water. For TSF Alternative 4, Whitlow Ranch Dam is the first downstream location where all tailings seepage reaches the surface, and as such is considered a valuable location for monitoring potential tailings seepage impacts.

Tailings Storage Facility - Alternative 4

For TSF Alternative 4, tailings would be pumped as thickened slurry to the Silver King site and then further dewatered with pressure filters at a filter plant. The scavenger and pyrite filtered tailings would be transported using a conveyance system from the filter plant to separate filtered tailings piles. The top of the tailings piles would be sloped into the hillside to limit surface water runoff over, and erosion of, the TSF slope. Downstream slopes would be progressively reclaimed and non-contact runoff would be diverted around the water collection dams when possible (KCB, 2018).

A more complete description of the TSF Alternative 4 design is described in the technical memorandum for solute modeling parameters prepared by Klohn Crippen Berger (KCB, 2018).

GoldSim Seepage Transport Model

Contaminant Transport Module

The CT Module extension of GoldSim is a mass transport model, not a flow model. As such, it does not directly solve for the movement of water through the modeled environmental system (GoldSim, 2017). The CT Module relies on user-specified flow rates for all flows into and out of aquifers, and therefore the velocity at which water moves through the media depends on the flow rates and volume of the available pore space in the aquifer pathways.

The CT Module has been used to develop an advection-dispersion mass flux model with mixing of inflow and outflow components to estimate the transport of chemical constituents through time. Mechanical dispersion of the constituents occurs as a function of the porosity and tortuosity of the aquifer, and the dispersivity values specified in the model. The dispersivity values assigned to aquifer element pathways was estimated as 10% of aquifer subdomain length based on Gelhar and others (1992).

Model Domain

The model domain includes nine alluvial aquifer subdomains, as shown on **Figure 3**. In the model, seepage from the TSF enters the Silver King Wash, Happy Camp Canyon East and West, and Potts Canyon subdomains immediately downstream of the TSF footprint. Water flowing through the Happy Camp West subdomain enters the Happy Camp East subdomain. Water from the Silver King Wash, Happy Camp Canyon (East and West), and Potts Canyon subdomains enters the Queen Creek 5, 4, and 3 subdomains, respectively. Water that passes through the Queen Creek 3 subdomain flows into the Queen Creek 2 subdomain before reaching the Queen Creek 1 subdomain. Once mixed in the Queen Creek 1 subdomain, the water is conveyed through Whitlow Ranch Dam.

The nine alluvial aquifers subdomains have unique geometries; the areas, lengths, and average widths were estimated based on polygon areas for the alluvium using ArcGIS. Cross-sectional areas and saturated thicknesses of the aquifer subdomains were estimated based on Darcy's Law. Calculations were made using the average flow rate through the subdomains, and hydraulic conductivities of approximately 500 feet per day (ft/day) in the canyons and washes and 1,000 ft/day in Queen Creek, based on hydraulic testing conducted in the alluvium (M&A, 2017c). The dimensions of the aquifer subdomains used in the seepage transport model are given in **Table 1**.

Materials and Parameters

Water

The GoldSim CT Module requires properties for a reference fluid and the flow medium for models. The reference fluid was specified as water, with a diffusivity of 1E-9 meters squared per second. For the seepage transport model, the diffusivity reduction formula, relative diffusivities, and solubility input parameters did not apply as the media was fully saturated and the constituent concentrations did not approach solubility limits.

Alluvium

The medium in the model was native alluvium, with an assumed advective porosity of 0.15 and a dry (bulk) density of 2,000 kilograms per cubic meter based on reference estimates (Sharma, 1997). The tortuosity was estimated as the cube root of the porosity, with a value of 0.53 (GoldSim, 2017). Partition coefficients were not specified as it was assumed that the transport of constituents was conservative (i.e. constituents do not sorb onto the alluvium).

Water Budget

Water enters the aquifer subdomains as recharge, groundwater underflow, and seepage from the TSF impoundment. Water exits the aquifer subdomains as groundwater evapotranspiration (GET), as flow passing into the next aquifer subdomain immediately downstream, and at Whitlow Ranch Dam which is the ultimate discharge point for groundwater exiting the Superior Basin (M&A, 2017b).

Descriptions of aquifer inflows and outflows are presented below. A summary of water budget components used in the Alternative 4 model is given in **Table 2**. A complete water balance for the Superior Basin was included in the conceptual hydrogeologic model report for Near West (M&A, 2017b).

Inflows

Recharge

Recharge includes inflow from precipitation occurring within aquifer subbasins. Estimates of recharge for model subbasins were based on total recharge for the Near West study area (M&A, 2017b). Total recharge within the Near West study area was approximated using a method developed by Anderson and others (1992) that incorporates precipitation, basin area, and elevation. Average annual precipitation was estimated using the PRISM model (PRISM Climate Group, 2017).

The total recharge for the Near West study area was allocated to Alternative 4 model subbasins based on the fractional area of each subbasin within the study area. Once allocated, recharge within each subbasin was then subdivided into focused recharge—identified simply as “recharge” within the model—and diffuse recharge classified as groundwater underflow in the model. The model assumed 75% of recharge to be focused recharge and 25% to be diffuse recharge based on estimates provided by Meixner and others (2016). Recharge estimates for the aquifer subdomains are provided in **Table 2**.

Groundwater Underflow

Groundwater underflow includes inflow to aquifer subdomains from the movement of groundwater originating from upstream portions of aquifer subbasins or from areas outside of the model domain. As indicated in *Recharge* above, the seepage transport model assumed 25% of total recharge to be contributions to groundwater underflow.

Additional underflow into Queen Creek aquifers from upstream basin areas outside of the model domain to the south of Queen Creek and to the east of Silver King Wash represented a significant portion of inflow. Estimates of groundwater underflows are provided in **Table 2**.

TSF Seepage

For the LOM period, the TSF seepage rate was calculated as the average rate reported for mine operation in the Alternative 4 engineering design (KCB, 2018). The average LOM seepage rate, equal to approximately 0.60 acre-feet per year (af/yr), was then evenly distributed between the four downstream drainage pathways: Silver King Wash, Potts Canyon, Happy Camp Canyon East and Happy Camp Canyon West.

Post-closure seepage rates were based on values reported in the embankment oxidation tailings chemistry analysis (Rio Tinto, 2018). Total tailings seepage increases during the modeled post-closure period as meteoric precipitation wets the initially dry tailings impoundment. During this period, seepage increases from approximately 13 to 24 af/yr (Rio Tinto, 2018). Post-closure seepage was divided evenly between the four downstream drainage pathways.

Seepage estimates included in the model are presented in **Table 2** and summarized below.

Aquifer Subdomain	Seepage Rates During Life of Mine (Years 0 – 41) ¹	
	Seepage (af/yr ²)	Seepage (gpm ³)
Silver King Wash	0.15	0.093
Happy Camp East	0.15	0.093
Happy Camp West	0.15	0.093
Potts Canyon	0.15	0.093

¹ Post-closure (years 42 – 245) total seepage rate varies annually from 13.6 to 23.8 af/yr (Rio Tinto, 2018)

² af/yr = acre-feet per year

³ gpm = gallons per minute

Outflows

Groundwater Evapotranspiration (GET)

GET includes outflow from aquifer subdomains due to evaporation and transpiration. GET occurs after inflows from all sources—recharge, groundwater underflow, TSF seepage, and discharge from upstream alluvial reaches—have mixed in the aquifer subdomain; consequently, the masses of chemical constituents are removed in proportion to their concentrations in the aquifer subdomains after mixing. GET was estimated for the subdomains in the Near West study area and the areas east of Near West using the water balance developed for the Near West conceptual model report (M&A, 2017b). Total GET was distributed across the Near West study area based on the fractional areas of the subdomains. Estimates of GET are given in **Table 2**.

Outflow to Downstream Aquifer Subdomain

After GET is removed from each aquifer subdomain, the remaining water flows into the next adjacent subdomain located immediately downstream. The flow direction between aquifer subdomains is indicated with blue arrows on **Figure 3**. Outflow from the upstream subdomain becomes inflow to the downstream subdomain. Water discharging from the last aquifer subdomain, Queen Creek 1, passes through Whitlow Ranch Dam and ultimately terminates in a sink pathway cell. The outflow at Whitlow Ranch Dam is based on median baseflow conditions (M&A, 2017b). This is a conservative assumption, since average baseflow is higher and would further dilute aquifer discharge at Whitlow Ranch Dam. The outflow values used in the Alternative 4 model for each subdomain are given in **Table 2**.

Timing of Seepage Transit from TSF to Model Domain

The Alternative 4 footprint lies directly above four aquifer subdomains included in the model—Potts Canyon, Happy Camp Canyon East, Happy Camp Canyon West, and Silver King Wash. As a result, the time required for seepage leaving the tailings to enter the aquifer subdomains should be minimal, and no transit delay was incorporated into the model.

Chemical Constituents

A total of 30 chemical constituents were included in process circuit and embankment oxidation chemistry models developed for LOM and post-closure years (Enchemica, 2018 and Rio Tinto, 2018). All of the constituents were included in the seepage transport model. The constituents include common and trace metals, as well as bicarbonate, nitrate-N, sulfate and total dissolved solids, and are shown in **Tables 3 through 9**.

Concentration and Mass Flux of Constituents

The CT Module requires mass and flow inputs in order to simulate the movement of constituent mass through the model domain. Constituent concentrations can be monitored at discrete locations through time based on the amount of fluid (water) and constituent mass at the monitoring location.

In order to simplify the modeling approach, the seepage transport model developed for Alternative 4 assumed a mass flux of zero milligrams per day from all natural waters—i.e. meteoric precipitation and groundwater. The only mass flux included in the model was derived from TSF seepage.

The last step of the analysis was to add background concentrations of natural waters to modeled concentrations, in order to estimate total predicted concentrations downstream of the tailings impoundment during and after mining. Background concentrations were determined by calculating the median constituent concentrations from samples collected at well DS17-17, located within the Queen Creek 3 subdomain, and at Whitlow Ranch Dam. Summaries of historical water quality samples collected at DS17-17 and Whitlow Ranch Dam are given in **Tables 3 and 4**, respectively. Median background concentrations and applicable water quality standards for each location are also shown included in the tables.

Tailings seepage concentrations for LOM years were based on a tailings circuit predictive model for the entire TSF during mine operations (Enchemica, 2018). Tailings concentrations for post-closure years were based on a second model, which analyzed the effects of weathering processes, such as sulfide oxidation, on the TSF embankment over

time (Rio Tinto, 2018). As both the process circuit and weathering analyses were used to construct the tailings seepage chemistry for the GoldSim model, slight differences were observed in solute concentrations between the end of the LOM (year 41) and beginning of post-closure (year 42). These differences were addressed in a conservative manner by maintaining the LOM concentration until it was exceeded by the post-closure concentration. If the concentration at the end of LOM (year 42) was not exceeded during post-closure, the LOM concentration was maintained through the end of the model period (year 245).

The constituent concentrations of TSF seepage during the 245-year model period are given in **Table 5**. The mass fluxes entering Potts Canyon, Happy Camp Canyon East and West, and Silver King Wash were calculated by multiplying the constituent concentrations shown in **Tables 5** by estimated seepage rates for the LOM and post-closure periods (see *TSF Seepage, Table 2* and Rio Tinto, 2018).

Model Simulation Settings

The model was designed to simulate 245 years after the start of mining, which includes the 41 years of planned LOM and 204 additional years following closure. Basic time steps of 0.1 years (36.525 days) were used for model calculations, with reporting steps of 1 year. All aquifer subdomain elements were given the maximum number of cell divisions (100 cells) in order to minimize numerical dispersion in model calculations.

Conservative Assumptions

The modeling approach includes many assumptions because detailed information is not available for this site. The model is intentionally simple and intended to be used as a tool for comparison between the proposed TSF alternatives. Some assumptions are conservative and result in overestimates of modeled concentrations from TSF seepage.

The flow rate used at Whitlow Ranch Dam is based on median baseflow conditions. Average baseflow includes periods of higher flow associated with rainfall events, and would be expected to further reduce concentrations observed at Whitlow Ranch Dam. In addition, hardness-dependent surface water standards at Whitlow Ranch Dam (cadmium, copper, lead, nickel, and zinc) were calculated using the lowest available hardness measurement at the dam; using average or median hardness would increase the calculated thresholds for the hardness-dependent standards.

Differences in tailings seepage concentrations generated for the LOM and post-closure periods were addressed using a conservative approach. When circuit chemistry seepage concentrations at the end of the LOM (year 41) were higher than embankment oxidation

concentrations at the beginning of post-closure (year 42), the higher LOM concentration was maintained through the end of the model period (year 245) or until it was exceeded by post-closure concentrations.

Due to assumptions described above, predicted constituent concentrations should not be considered definitive, and arguably contribute more value in relative rather than absolute terms, through comparisons with other TSF alternatives.

Results

Modeled Constituent Concentrations

Modeled constituent concentrations in groundwater downstream of the TSF were monitored in the Queen Creek 3 subdomain. The results—which show the contributions to solute concentrations from TSF seepage, and do not include background concentrations of local groundwater—are given in **Table 6**. Following mixing and transport in the model, constituent concentrations downstream of the TSF decreased by approximately 99.9% during LOM, and by approximately 98.2 to 99.9% during post-closure, compared to initial tailings seepage concentrations (**Tables 5 and 6**).

Modeled constituent concentrations in surface water downstream of the TSF were monitored at Whitlow Ranch Dam. The results are provided in **Table 7**. Following transport and mixing in the model, constituent concentrations decreased by approximately 99.9% during LOM, and by approximately 99.1 to 99.9% following closure, compared to initial tailings concentrations (**Tables 5 and 7**).

Predicted Total Constituent Concentrations

In order to estimate total constituent concentrations, median background concentrations derived from water quality samples from well DS17-17 (**Table 3**), located within Queen Creek 3, and from Whitlow Ranch Dam (**Table 4**) were added to modeled concentrations. The total predicted constituent concentrations due to natural background and TSF seepage at Queen Creek 3 after the start of mining are given in **Table 8**. Predicted total concentrations at Whitlow Ranch Dam are given in **Table 9**.

Comparison to Water Quality Standards

Modeled concentrations are compared to promulgated water quality standards to provide an indication of potential chemical constituents of concern and to assess the relative

performance of different TSF alternatives. Model results are useful indicators for comparative purposes, but are not considered definitive or final.

Water quality standards for the Queen Creek 3 subdomain are the Arizona Department of Environmental Quality (ADEQ) Numeric Aquifer Water Quality Standards (AWQS) (ADEQ, 2016). Water quality standards at Whitlow Ranch Dam are the ADEQ Numeric Surface Water Quality Standards (SWQS) for the aquatic and wildlife warm (chronic) designation (ADEQ, 2016), which are the most restrictive standards that apply at the dam. Five of the modeled constituents—cadmium, copper, lead, nickel, and zinc—have surface water standards that are hardness dependent and were conservatively calculated (worst case) by using the lowest available hardness value recorded at Whitlow Ranch Dam (307 milligrams per liter calcium carbonate on 8/25/2017). The regulatory standards for the chemical constituents are given in **Tables 3 and 4** and are included for comparison with calculated values in **Tables 6 through 9**.

At the Queen Creek 3 groundwater monitoring location, none of the constituent concentrations in the model results (with zero background concentration) or in the predicted concentrations (with background concentrations included) are shown to occur above AWQS at any time during the model period.

At Whitlow Ranch Dam, only selenium is shown to occur above SWQS during the model period, which occurs in both model results (with zero background concentration) and predicted concentrations (with background concentrations included).

Discussion and Conclusions

Modeled concentrations are compared to promulgated water quality standards to provide an indication of potential chemical constituents of concern and to assess the relative performance of different TSF alternatives against standards. Model results are useful indicators for comparative purposes, but are not considered definitive or final.

Based on the Alternative 4 engineering design report (KCB, 2018) and an embankment oxidation analysis (Rio Tinto, 2018), the rate of TSF seepage is minimal—approximately 0.6 af/yr during the LOM and 13 to 24 af/yr during post-closure. As a result of increased seepage following mine closure, model results indicate that concentrations in groundwater and surface water are higher during post-closure than during mine life.

Constituent concentrations were monitored at the Queen Creek 3 subdomain and Whitlow Ranch Dam. When tailings seepage reached these locations, the constituent concentrations had decreased by approximately 98.2% to 99.9% from initial tailings concentrations. Modeled concentrations were added to background concentrations at Queen Creek 3 and

Whitlow Ranch Dam in order to predict total constituent concentrations at these locations. The results indicate that aquifer and surface water quality would be beneath standards with the exception of selenium at Whitlow Ranch Dam during some of the modeled period.

The TSF alternatives are located at four different sites and incorporate differing technologies, but for the purpose of comparing the alternatives, only the minimum seepage controls required for geotechnical stability were incorporated. Additional seepage collection controls will be incorporated into future TSF designs.

The modeled flow at Whitlow Ranch Dam was based on median baseflow conditions. Average conditions, which are influenced by periods of higher flow associated with rainfall events, would be expected to be greater than the flow used in the model, and would further reduce concentrations. Therefore, the model results may overestimate constituent concentrations. Additionally, conservative methods applied to the determination of tailings chemistry incorporated in the model may also overestimate actual constituent concentrations.

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Table 1. Dimensions of Aquifer Subdomains

Aquifer Subdomain	Length (ft)	Area ^a (ft ²)	Average Width ^b (ft)	Saturated Thickness ^c (ft)	Cross Sectional Area ^c (ft ²)
Silver King	20,100	10,219,800	510	1.1	600
Happy Camp E	23,700	14,186,100	600	0.2	100
Happy Camp W	12,300	6,052,900	490	0.1	100
Potts Canyon	23,400	8,340,600	360	6.3	2,300
Queen Creek 5	3,500	1,082,900	310	2.2	700
Queen Creek 4	9,900	5,398,500	550	3.4	1,900
Queen Creek 3	15,700	17,899,700	1,140	5.6	6,400
Queen Creek 2	6,400	5,656,700	880	17.1	15,000
Queen Creek 1	6,300	8,328,000	1,320	12.1	15,900

Notes:

^a Calculated based on polygon area of each subdomain in ArcGIS

^b Calculated by dividing aquifer polygon area by width

^c Based on Darcy's Law using the average flow rate through the subdomain during Life of Mine

Table 2. Water Budget Components

Aquifer Subdomain	INFLOW		OUTFLOW	
	Source	af/yr	Source	af/yr
Silver King Wash	Recharge	68	Groundwater Evapotranspiration (GET)	57
	Underflow	23	Discharge to Queen Creek 5	34.15
	TSF Seepage during Life of Mine (LOM)	0.15		
Happy Camp East	Recharge	20	Groundwater Evapotranspiration (GET)	25
	Underflow	7	Discharge to Queen Creek 4	2.3
	TSF Seepage during Life of Mine (LOM)	0.15		
	Happy Camp W Discharge	0.15		
Happy Camp West	Recharge	10	Groundwater Evapotranspiration (GET)	13
	Underflow	3	Discharge to Happy Camp E	0.15
	TSF Seepage during Life of Mine (LOM)	0.15		
Potts Canyon	Recharge	169	Groundwater Evapotranspiration (GET)	81
	Underflow	57	Discharge to Queen Creek 3	145.15
	TSF Seepage during Life of Mine (LOM)	0.15		
Queen Creek 5	Recharge	1.5	Groundwater Evapotranspiration (GET)	1
	Underflow	0.5	Discharge to Queen Creek 4	35.15
	Silver King Wash Discharge	34.15		
Queen Creek 4	Recharge	9	Groundwater Evapotranspiration (GET)	4
	Underflow	123	Discharge to Queen Creek 3	165.45
	Queen Creek 5 Discharge	35.15		
	Happy Canyon E Discharge	2.30		
Queen Creek 3	Recharge	89	Groundwater Evapotranspiration (GET)	32
	Underflow	88	Discharge to Queen Creek 2	455.6
	Queen Creek 4 Discharge	165.45		
	Potts Canyon Discharge	145.15		
Queen Creek 2	Recharge	225	Groundwater Evapotranspiration (GET)	80
	Underflow	122	Discharge to Queen Creek 1	722.6
	Queen Creek 3 Discharge	455.6		
Queen Creek 1	Recharge	30	Groundwater Evapotranspiration (GET)	11
	Underflow	53	Discharge to Whitlow Ranch Dam (WRD)	794.6
	Queen Creek 2 Discharge	722.6		

Notes:

1. Recharge, underflow and GET estimates based conceptual model report (M&A, 2017a) and subbasin areas
2. TSF seepage estimates during Life of Mine based on three-dimensional steady-state groundwater flow model (M&A, 2018)
3. During Post-Closure, total TSF seepage ranges from 13.6 to 23.8 af/yr and Queen Creek 1 discharge ranges from 807.6 to 817.8 af/yr

Table 3. Median Background Concentrations and Water Quality Standards at Well DS17-17 in Queen Creek 3 Subdomain

Sample Date	Al DIS mg/L	Sb DIS mg/L	As DIS mg/L	Ba DIS mg/L	Be DIS mg/L	HCO3 TOT mg/L	B DIS mg/L	Cd DIS mg/L	Ca DIS mg/L	Cl TOT mg/L	Cr DIS mg/L	Co DIS mg/L	Cu DIS mg/L	F TOT mg/L	Fe DIS mg/L	Pb DIS mg/L	Mg DIS mg/L	Mn DIS mg/L	Mo DIS mg/L	Ni DIS mg/L	NO3-N TOT ^a mg/L	K DIS mg/L	Se TOT mg/L	Si DIS mg/L	Ag DIS mg/L	Na DIS mg/L	SO4 TOT mg/L	TI DIS mg/L	Zn DIS mg/L	TDS DIS mg/L
2/22/2018	<0.05	<0.00023	0.0010	0.0251	<0.0017	437	0.073	<0.000063	102	26.1	<0.0020	<0.0016	0.00056	0.624	<0.056	<0.00011	21.6	<0.0034	<0.003	<0.0023		2.47	0.0004	53.5	<0.000061	60.0	129	<0.00008	<0.005	576
1/16/2018	<0.04	<0.000033	0.0009	0.0201	<0.0010	414	0.074	<0.000038	102	27.3	<0.0019	<0.0013	0.00161	0.578	<0.045	0.00039	22.5	0.0079	<0.003	<0.0027		2.79	0.0004	48.2	<0.000036	58.4	133	<0.00003	0.016	589
12/6/2017	<0.04	0.00022	0.0013	0.0222	<0.0010	351	0.069	<0.000038	84.0	24.7	<0.0019	<0.0013	0.00048	0.553	<0.045	<0.000065	21.2	<0.0049	<0.003	<0.0027		3.39	0.0004	42.9	<0.000036	49.5	111	<0.00003	<0.003	477
11/10/2017	<0.04	0.00021	0.0012	0.0261	<0.0010	342	0.070	<0.000038	103	29.4	<0.0019	<0.0013	0.00057	0.529	<0.045	<0.000065	26.5	<0.0049	<0.003	<0.0027		3.49	0.0005	43.5	<0.000036	52.3	162	<0.00003	<0.003	554
10/10/2017	<0.04	0.00017	0.0013	0.0284	<0.0010	340	0.068	0.00006	99.6	29.7	<0.0019	<0.0013	0.00076	0.554	<0.045	<0.00013	26.0	<0.0049	<0.003	<0.0027		3.65	0.0009	42.5	<0.000036	51.2	176	<0.00006	0.0030	606
9/11/2017	<0.04	0.00023	0.0013	0.0318	<0.0010	327	0.068	<0.000038	111	36.9	<0.0019	<0.0013	0.00075	0.388	<0.045	<0.000065	29.0	<0.0049	<0.003	<0.0027		3.70	0.0011	42.8	<0.000036	53.3	218	<0.00003	0.0040	657
8/20/2017	<0.04	0.00026		0.0254	<0.0010	316	0.069	<0.000038	100	31.7	<0.0019	<0.0013	0.00085	0.463	<0.045	<0.000065	25.7	<0.0049	<0.003	<0.0027			0.0012	40.6	<0.000036		173	<0.00003	0.018	583
8/19/2017	<0.04	0.00021		0.0274	<0.0010	316	0.069	<0.000038	101	32.2	<0.0019	<0.0013	0.00098	0.432	<0.045	<0.000065	26.3	<0.0049	<0.003	<0.0027			0.0009	40.9	<0.000036		180	<0.00003	0.025	591
5/19/2017	<0.03	0.00020	0.0014	0.0312	<0.0007	334	0.072	<0.000038		34.4	<0.0019	<0.0013	0.00106	0.457	<0.045	<0.000065		<0.0049	<0.003	<0.0027			0.0015	41.6	<0.000036		206	<0.00003	0.0090	641

Median =	0.04	0.00021	0.0013	0.0261	0.0010	340	0.069	0.00004	101.5	29.7	0.0019	0.0013	0.00076	0.529	0.045	0.000065	25.9	0.0049	0.003	0.0027	0.38	3.44	0.0009	42.8	0.000036	52.8	173	0.00003	0.005	589
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Aquifer WQ Standard =		0.006	0.05	2	0.004			0.005			0.1			4.0		0.05			0.1	10	0.05					0.002	
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Notes:

- ^a No available data for well DS17-17. NO3-N median value calculated as median of three samples collected from Bear Tank and Benson Springs between November 2014 and March 2015
- 1. Values less than laboratory detection limit ("non-detects") assumed equal to detection limit for calculation of median concentrations
- 2. Dissolved (DIS) and total (TOT) constituent concentrations shown based on available data
- 3. Aquifer WQ Standard = Arizona Department of Environmental Quality Numeric Aquifer Water Quality Standards (Arizona Administrative Code - Title 18, Ch. 11, Art. 4, Sup. 16-4, 2016)
- 4. mg/L = milligrams per liter

Table 4. Median Background Concentrations and Water Quality Standards at Whitlow Ranch Dam

Sample Date	Al DIS mg/L	Sb DIS mg/L	As DIS mg/L	Ba DIS mg/L	Be DIS mg/L	HCO3 TOT mg/L	B DIS mg/L	Cd DIS mg/L	Ca DIS mg/L	Cl TOT mg/L	Cr DIS mg/L	Co DIS mg/L	Cu DIS mg/L	F TOT mg/L	Fe DIS mg/L	Pb DIS mg/L	Mg DIS mg/L	Mn DIS mg/L	Mo DIS mg/L	Ni DIS mg/L	NO3-N TOT mg/L	K DIS mg/L	Se TOT mg/L	Si DIS mg/L	Ag DIS mg/L	Na DIS mg/L	SO4 TOT mg/L	Tl DIS mg/L	Zn DIS mg/L	TDS DIS mg/L
12/7/2017	<0.04	0.00048	0.0014	0.0300	<0.0010	367	0.054	0.00004	104.0	23.5	<0.0019	<0.0013	0.00102	0.369	0.045	0.00011	25.5	0.017	<0.003	<0.0027		3.0	0.0004	39.3	<0.000036	38.8	132	<0.00003	0.0040	524
11/15/2017	<0.04	0.00046	0.0016	0.0259	<0.0010	334	0.050	<0.000038	95.0	22.3	<0.0019	<0.0013	0.00100	0.369	0.045	0.00013	22.8	0.016	<0.003	<0.0027		2.9	0.0006	35.5	<0.000072	36.0	119	<0.00003	<0.003	500
10/18/2017	<0.04	0.00045	0.0025	0.0512	<0.0010	351	0.053	0.00005	90.3	22.0	<0.0019	<0.0013	0.0008	0.377	0.180	<0.000065	22.4	0.399	<0.003	<0.0027		3.1	0.0007	36.5	<0.000036	35.7	111	<0.00003	0.0050	495
9/27/2017	<0.04	0.00038	0.0025	0.0311	<0.0010	331	0.050	<0.000038	89.5	21.1	<0.0019	<0.0013	0.0007	0.407	0.064	<0.000065	21.5	0.193	<0.003	<0.0027		2.8	0.0006	34.4	<0.000036	35.6	108	<0.00003	0.0030	490
8/25/2017	<0.04	0.00056	0.00359	0.0345	<0.0010	327	0.047	<0.000038	87.5	21.9	<0.0019	<0.0013	0.0010	0.435	0.047	<0.000065	21.4	0.276	<0.003	<0.0027		3.0	0.0007	33.5	<0.000036	34.8	113	<0.00003	<0.003	494
6/29/2017	<0.04	0.00035	0.0017	0.0284	<0.0010	285	0.050	0.00005		21.0	<0.0019	<0.0013	0.00130	0.417	0.045	<0.000065		0.028	<0.003	<0.0027			0.0008	34.4	<0.000036		112	<0.00003	<0.003	491
3/23/2017	0.040	0.00051	0.0026	0.0509	<0.0010	320	0.055			21.2	<0.0015	<0.0010	0.00398	0.467	0.104	0.00030		0.152	<0.003	<0.0026			0.0011	36.6	<0.000036		136	<0.00003	<0.003	632
12/9/2016	<0.03	0.00041	0.0019	0.0321	<0.0010	336	0.057	<0.000021		26.2	<0.0015	<0.0010	<0.0026	0.344	0.079	0.00012		0.059	<0.003	<0.0026			0.0007	37.4	<0.000025		142	<0.000034	<0.003	546
7/22/2016	<0.03	0.00056	0.0024	0.0348	<0.0010	348	0.058			24.0	<0.0015	<0.0010	<0.0026	0.327	0.039	<0.000075		0.117	<0.004	<0.0026			0.0009	39.1	<0.000025		133	<0.000034	<0.003	531
4/14/2016	<0.0364	0.00061	0.0020	0.035	<0.00057	348	0.067	0.00003		26.0	<0.00076	<0.0019	<0.0023	0.356	0.049	<0.000076		0.089	<0.0055	<0.0037			0.0010	40.5	<0.000025		141	<0.000034	<0.0039	558
2/12/2016	<0.04	0.00060	0.0024	0.0407	<0.0006	387	0.065	<0.000072		32.6	<0.0008	<0.0019	<0.0023	0.354	0.048	<0.000031		0.220	<0.005	<0.0037			0.0008	37.4	<0.000021		182	<0.000026	<0.004	612
10/20/2015	<0.04	0.00057	0.0025	0.0412	<0.0009	346	0.064	<0.000072		28.8	<0.0010	<0.0019	<0.0023	0.433	0.048	0.00006		0.258	<0.005	<0.0037			<0.0006	39.3	<0.000021		136	<0.000026	<0.004	566
9/9/2015	<0.0364	0.00061	0.0039	0.0438	<0.00095	350	0.062	<0.000073		28.1	<0.001	<0.0019	<0.0023	0.425	0.057	0.00006		0.500	<0.0055	<0.0037			<0.00062	38.8	<0.000021		142	<0.000026	<0.0039	580
5/13/2015	<0.04	0.00057	0.0020	0.0357	<0.0009	328	0.061	<0.000072		27.4	<0.0018	<0.0008	<0.0023	0.497	0.026	0.00010		0.150	<0.005	<0.0028			<0.0006	37.8	<0.000021		142	<0.000026	<0.003	570
3/4/2015	0.027	0.00052	0.0017	0.037	<0.00020	342	0.068	<0.00025		28.0	<0.00050	<0.00050	0.0020	0.43	0.024	<0.00050		0.049	0.0016	<0.0016	1.9		0.0007	37.0	<0.00050		150	<0.00050	<0.0025	560

Median = 0.04 0.00052 0.0024 0.0350 0.0010 342 0.057 0.00005 90.3 24.0 0.0015 0.0013 0.00230 0.407 0.048 0.000075 22.4 0.1500 0.003 0.0027 1.90 2.95 0.0007 37.4 0.000036 35.7 136 0.00003 0.003 546

Surface WQ Standard = 0.03000 0.1500 0.00512^a 0.02335^a 1.000 0.00833^a 0.13433^a 0.0020 0.150000 0.3031^b

Notes:

^a Cd, Cu, Pb, Ni and Zn standards are hardness dependent and were calculated using lowest (most stringent) hardness value recorded for Whitlow Ranch Dam (307 mg/L CaCO₃ on 8/25/2017)

1. Values less than laboratory detection limit ("non-detects") assumed equal to detection limit for calculation of median concentrations

2. Dissolved (DIS) and total (TOT) species concentrations shown based on Arizona water quality standards requirements and available data

3. Surface WQ Standard = Arizona Department of Environmental Quality Water Quality Standard for "Aquatic and wildlife warm" (A&ww) water with chronic exposure (Arizona Administrative Code - Title 18, Ch. 11, Sup. 16-4, 2016)

4. mg/L = milligrams per liter

Table 5. Tailings Seepage Concentrations - Alternative 4

Years since Mine Start	Al	Sb	As	Ba	Be	HCO3	B	Cd	Ca	Cl	Co	Cu	F	Fe	Pb	Mg	Mn	Mo	Ni	NO3-N	K	Se	Si	Ag	Na	SO4	Tl	Zn	TDS	
	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L		
1	0.077	0.00030	0.0056	0.014	0.0006	31	0.033	0.00003	11.3	2.6	0.0010	0.0011	0.0794	0.140	0.002	0.00011	4.3	0.023	0.0017	0.002	3.40	4.3	0.0003	7.1	0.00002	2.8	9	0.00002	0.003	60
2	0.135	0.00031	0.0056	0.014	0.0006	30	0.032	0.00004	12.4	2.6	0.0010	0.0021	0.1873	0.138	0.002	0.00012	4.4	0.034	0.0020	0.004	3.38	4.4	0.0005	7.1	0.00002	2.8	14	0.00002	0.006	66
3	0.198	0.00032	0.0055	0.014	0.0006	30	0.032	0.00006	13.6	2.6	0.0010	0.0032	0.1925	0.137	0.002	0.00012	4.6	0.047	0.0023	0.006	3.34	4.6	0.0007	7.0	0.00002	2.9	18	0.00002	0.009	72
4	0.261	0.00032	0.0054	0.014	0.0006	29	0.031	0.00008	14.6	2.5	0.0010	0.0043	0.1926	0.133	0.002	0.00012	4.7	0.060	0.0026	0.008	3.24	4.6	0.0008	6.9	0.00002	2.9	23	0.00002	0.012	77
5	0.325	0.00033	0.0052	0.014	0.0007	28	0.030	0.00010	15.7	2.4	0.0010	0.0054	0.1927	0.129	0.002	0.00012	4.8	0.072	0.0030	0.010	3.14	4.7	0.0010	6.7	0.00002	2.9	28	0.00002	0.015	82
6	0.389	0.00034	0.0051	0.014	0.0007	27	0.030	0.00011	16.8	2.4	0.0010	0.0065	0.1928	0.127	0.002	0.00013	4.9	0.085	0.0033	0.012	3.09	4.8	0.0011	6.6	0.00002	2.9	33	0.00002	0.018	88
7	0.464	0.00035	0.0050	0.014	0.0007	27	0.029	0.00014	18.2	2.3	0.0010	0.0078	0.1929	0.124	0.002	0.00013	5.1	0.100	0.0036	0.015	3.02	5.0	0.0013	6.6	0.00002	3.0	39	0.00002	0.022	95
8	0.554	0.00036	0.0049	0.014	0.0008	26	0.029	0.00016	19.8	2.3	0.0009	0.0094	0.1931	0.121	0.002	0.00013	5.3	0.118	0.0041	0.018	2.94	5.1	0.0015	6.5	0.00002	3.0	45	0.00003	0.027	103
9	0.645	0.00037	0.0048	0.014	0.0008	25	0.028	0.00019	21.5	2.2	0.0009	0.0109	0.1933	0.117	0.002	0.00014	5.5	0.136	0.0045	0.021	2.86	5.3	0.0018	6.3	0.00002	3.1	52	0.00003	0.031	112
10	0.737	0.00038	0.0046	0.014	0.0009	24	0.027	0.00021	23.1	2.1	0.0009	0.0125	0.1935	0.114	0.002	0.00014	5.7	0.155	0.0050	0.024	2.78	5.5	0.0020	6.2	0.00002	3.1	59	0.00003	0.036	120
11	0.820	0.00040	0.0045	0.014	0.0009	23	0.027	0.00024	24.6	2.1	0.0009	0.0140	0.1937	0.111	0.002	0.00015	5.9	0.171	0.0054	0.027	2.70	5.6	0.0022	6.1	0.00002	3.2	66	0.00003	0.040	128
12	0.888	0.00040	0.0044	0.014	0.0009	22	0.026	0.00025	25.8	2.0	0.0009	0.0152	0.1939	0.108	0.002	0.00015	6.0	0.185	0.0057	0.029	2.64	5.8	0.0024	6.0	0.00002	3.2	71	0.00003	0.043	134
13	0.957	0.00041	0.0043	0.014	0.0010	21	0.025	0.00027	27.1	2.0	0.0009	0.0163	0.1942	0.106	0.002	0.00015	6.2	0.198	0.0061	0.031	2.57	5.9	0.0026	6.0	0.00002	3.2	76	0.00003	0.047	140
14	1.025	0.00042	0.0042	0.014	0.0010	21	0.025	0.00029	28.3	1.9	0.0009	0.0175	0.1944	0.103	0.002	0.00016	6.3	0.212	0.0064	0.033	2.51	6.0	0.0027	5.9	0.00002	3.3	81	0.00004	0.050	146
15	1.094	0.00043	0.0041	0.014	0.0010	20	0.024	0.00031	29.6	1.9	0.0008	0.0187	0.1947	0.100	0.002	0.00016	6.5	0.226	0.0067	0.036	2.45	6.1	0.0029	5.8	0.00002	3.3	86	0.00004	0.054	152
16	1.163	0.00044	0.0040	0.014	0.0011	19	0.024	0.00033	30.8	1.8	0.0008	0.0199	0.1950	0.098	0.002	0.00016	6.6	0.240	0.0071	0.038	2.38	6.3	0.0031	5.7	0.00002	3.4	92	0.00004	0.057	159
17	1.231	0.00045	0.0039	0.014	0.0011	18	0.023	0.00035	32.0	1.8	0.0008	0.0211	0.1953	0.095	0.002	0.00017	6.8	0.253	0.0074	0.040	2.32	6.4	0.0032	5.6	0.00002	3.4	97	0.00004	0.060	165
18	1.300	0.00046	0.0038	0.014	0.0011	18	0.023	0.00037	33.2	1.7	0.0008	0.0223	0.1957	0.092	0.002	0.00017	6.9	0.267	0.0077	0.042	2.26	6.5	0.0034	5.5	0.00002	3.4	102	0.00004	0.064	171
19	1.369	0.00047	0.0037	0.014	0.0012	17	0.022	0.00039	34.5	1.7	0.0008	0.0235	0.1961	0.090	0.002	0.00017	7.1	0.281	0.0081	0.045	2.19	6.6	0.0036	5.4	0.00001	3.5	107	0.00004	0.067	177
20	1.438	0.00048	0.0036	0.014	0.0012	16	0.022	0.00041	35.7	1.6	0.0008	0.0247	0.1966	0.087	0.002	0.00017	7.2	0.294	0.0084	0.047	2.13	6.8	0.0038	5.3	0.00001	3.5	113	0.00004	0.071	184
21	1.490	0.00049	0.0035	0.014	0.0012	16	0.021	0.00042	36.7	1.6	0.0008	0.0256	0.1971	0.085	0.002	0.00018	7.3	0.305	0.0087	0.049	2.08	6.9	0.0039	5.3	0.00001	3.5	117	0.00004	0.073	188
22	1.521	0.00049	0.0035	0.014	0.0013	15	0.021	0.00043	37.2	1.6	0.0008	0.0261	0.1973	0.084	0.002	0.00018	7.4	0.311	0.0088	0.050</td										

Table 5. Tailings Seepage Concentrations - Alternative 4

Years since Mine Start	Al	Sb	As	Ba	Be	HCO3	B	Cd	Ca	Cl	Co	Cu	F	Fe	Pb	Mg	Mn	Mo	Ni	NO3-N	K	Se	Si	Ag	Na	SO4	Tl	Zn	TDS	
	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	
67	1.309	0.02255	0.0194	0.014	0.0016	26	0.941	0.01589	516.3	103.1	0.0536	0.2266	0.2012	2.365	0.002	0.00367	278.7	3.980	0.9957	0.276	1.49	280.7	0.3392	4.5	0.06439	118.1	2768	0.00429	3.488	4106
68	1.309	0.02255	0.0195	0.014	0.0016	26	0.941	0.01588	516.3	103.0	0.0536	0.2266	0.2012	2.364	0.002	0.00367	278.9	3.977	0.9953	0.276	1.49	280.7	0.3390	4.5	0.06435	118.1	2768	0.00429	3.486	4106
69	1.309	0.02256	0.0195	0.014	0.0016	26	0.941	0.01588	516.3	103.0	0.0536	0.2265	0.2012	2.362	0.002	0.00367	279.1	3.975	0.9948	0.276	1.49	280.6	0.3389	4.5	0.06431	118.0	2769	0.00429	3.485	4107
70	1.309	0.02256	0.0195	0.014	0.0016	26	0.941	0.01587	516.3	102.9	0.0535	0.2265	0.2012	2.361	0.002	0.00367	279.3	3.972	0.9943	0.276	1.49	280.6	0.3388	4.5	0.06427	117.9	2769	0.00428	3.484	4108
71	1.309	0.02257	0.0195	0.014	0.0016	26	0.942	0.01586	516.3	102.8	0.0535	0.2265	0.2012	2.359	0.002	0.00367	279.4	3.970	0.9939	0.276	1.49	280.5	0.3387	4.5	0.06423	117.8	2770	0.00428	3.483	4108
72	1.309	0.02257	0.0195	0.014	0.0016	26	0.942	0.01586	516.3	102.8	0.0535	0.2265	0.2012	2.359	0.002	0.00367	279.5	3.969	0.9937	0.276	1.49	280.5	0.3387	4.5	0.06421	117.8	2770	0.00428	3.483	4108
73	1.309	0.02257	0.0195	0.014	0.0016	26	0.942	0.01585	516.3	102.7	0.0534	0.2263	0.2012	2.356	0.002	0.00367	279.6	3.965	0.9929	0.276	1.49	280.3	0.3385	4.5	0.06415	117.7	2770	0.00427	3.480	4108
74	1.309	0.02257	0.0195	0.014	0.0016	26	0.942	0.01584	516.3	102.6	0.0534	0.2262	0.2012	2.354	0.002	0.00367	279.7	3.961	0.9921	0.276	1.49	280.2	0.3382	4.5	0.06409	117.6	2770	0.00427	3.478	4108
75	1.309	0.02257	0.0195	0.014	0.0016	26	0.942	0.01583	516.3	102.5	0.0533	0.2261	0.2012	2.352	0.002	0.00367	279.8	3.957	0.9913	0.276	1.49	280.0	0.3380	4.5	0.06403	117.5	2770	0.00427	3.476	4108
76	1.309	0.02257	0.0196	0.014	0.0016	26	0.942	0.01582	516.3	102.4	0.0533	0.2260	0.2012	2.350	0.002	0.00367	279.9	3.954	0.9906	0.276	1.49	279.9	0.3378	4.5	0.06398	117.4	2771	0.00426	3.474	4108
77	1.309	0.02257	0.0196	0.014	0.0016	26	0.941	0.01581	516.3	102.4	0.0533	0.2260	0.2012	2.349	0.002	0.00367	279.9	3.953	0.9903	0.276	1.49	279.8	0.3377	4.5	0.06395	117.3	2770	0.00426	3.473	4107
78	1.309	0.02256	0.0196	0.014	0.0016	26	0.941	0.01580	516.4	102.3	0.0532	0.2258	0.2012	2.346	0.002	0.00367	279.9	3.948	0.9892	0.276	1.49	279.6	0.3374	4.5	0.06387	117.2	2770	0.00426	3.470	4107
79	1.309	0.02255	0.0196	0.014	0.0016	26	0.941	0.01578	516.4	102.1	0.0531	0.2256	0.2012	2.343	0.002	0.00367	279.9	3.943	0.9881	0.276	1.49	279.3	0.3371	4.5	0.06379	117.0	2770	0.00425	3.466	4106
80	1.309	0.02254	0.0196	0.014	0.0016	26	0.940	0.01576	516.4	102.0	0.0531	0.2254	0.2012	2.340	0.002	0.00367	279.9	3.937	0.9869	0.275	1.49	279.1	0.3367	4.5	0.06370	116.9	2769	0.00424	3.463	4105
81	1.309	0.02254	0.0196	0.014	0.0016	26	0.940	0.01575	516.5	101.9	0.0530	0.2253	0.2012	2.337	0.002	0.00367	279.9	3.933	0.9860	0.275	1.49	278.9	0.3364	4.5	0.06363	116.7	2769	0.00424	3.460	4104
82	1.309	0.02253	0.0196	0.014	0.0016	26	0.940	0.01574	516.5	101.8	0.0530	0.2252	0.2012	2.336	0.002	0.00367	279.9	3.931	0.9855	0.275	1.49	278.8	0.3363	4.5	0.06360	116.7	2769	0.00424	3.458	4104
83	1.309	0.02251	0.0196	0.014	0.0016	26	0.939	0.01572	516.6	101.7	0.0529	0.2249	0.2012	2.332	0.002	0.00367	279.8	3.925	0.9841	0.275	1.49	278.5	0.3358	4.5	0.06349	116.5	2768	0.00423	3.454	4102
84	1.309	0.02250	0.0196	0.014	0.0016	26	0.938	0.01570	516.6	101.5	0.0528	0.2246	0.2012	2.328	0.002	0.00367	279.7	3.918	0.9826	0.275	1.49	278.1	0.3354	4.5	0.06339	116.3	2767	0.00422	3.449	4101
85	1.309	0.02248	0.0196	0.014	0.0016	26	0.938	0.01568	516.7	101.3	0.0527	0.2244	0.2012	2.324	0.002	0.00366	279.6	3.912	0.9811	0.274	1.49	277.8	0.3349	4.5	0.06328	116.1	2766	0.00422	3.444	4099
86	1.309	0.02246	0.0195	0.014	0.0016	26	0.937	0.01566	516.8	101.2	0.0526	0.2241	0.2012	2.321	0.002	0.00366	279.5	3.906	0.9799	0.274	1.49	277.5	0.3345	4.5	0.06319	115.9	2766	0.00421	3.440	4097
87	1.309	0.02245	0.0195	0.014	0.0016	26	0.936	0.01565	516.8	101.1	0.0526	0.2240	0.2012	2.319	0.002	0.00366	279.4	3.903	0.9792	0.274	1.49	277.3	0.3343	4.5	0.					

Table 5. Tailings Seepage Concentrations - Alternative 4

Years since Mine Start	Al	Sb	As	Ba	Be	HCO3	B	Cd	Ca	Cl	Co	Cu	F	Fe	Pb	Mg	Mn	Mo	Ni	NO3-N	K	Se	Si	Ag	Na	SO4	Tl	Zn	TDS	
	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	
133	1.309	0.02092	0.0186	0.014	0.0016	26	0.872	0.01418	522.5	90.6	0.0471	0.2048	0.2012	2.079	0.002	0.00343	264.4	3.504	0.8841	0.252	1.49	253.2	0.3037	4.5	0.05661	103.8	2679	0.00377	3.123	3953
134	1.309	0.02089	0.0186	0.014	0.0016	26	0.870	0.01415	522.6	90.4	0.0470	0.2043	0.2012	2.072	0.002	0.00342	264.1	3.493	0.8817	0.252	1.49	252.6	0.3029	4.5	0.05644	103.5	2677	0.00376	3.115	3950
135	1.309	0.02086	0.0186	0.014	0.0016	26	0.869	0.01411	522.7	90.1	0.0469	0.2039	0.2012	2.066	0.002	0.00342	263.8	3.483	0.8793	0.251	1.49	252.0	0.3021	4.5	0.05628	103.2	2675	0.00375	3.107	3946
136	1.309	0.02083	0.0186	0.014	0.0016	26	0.868	0.01408	522.8	89.9	0.0468	0.2035	0.2012	2.062	0.002	0.00341	263.7	3.475	0.8775	0.251	1.49	251.5	0.3016	4.5	0.05615	103.0	2674	0.00374	3.102	3944
137	1.309	0.02083	0.0186	0.014	0.0016	26	0.867	0.01407	522.9	89.8	0.0467	0.2034	0.2012	2.059	0.002	0.00341	263.7	3.472	0.8767	0.251	1.49	251.4	0.3013	4.5	0.05609	102.9	2674	0.00374	3.099	3944
138	1.309	0.02080	0.0186	0.014	0.0016	26	0.866	0.01404	523.0	89.5	0.0466	0.2030	0.2012	2.054	0.002	0.00341	263.5	3.463	0.8746	0.250	1.49	250.8	0.3007	4.5	0.05594	102.6	2672	0.00373	3.092	3941
139	1.309	0.02077	0.0186	0.014	0.0016	26	0.865	0.01400	523.1	89.3	0.0464	0.2026	0.2012	2.048	0.002	0.00340	263.2	3.452	0.8722	0.250	1.49	250.3	0.2999	4.5	0.05577	102.3	2671	0.00371	3.085	3938
140	1.309	0.02074	0.0186	0.014	0.0016	26	0.864	0.01397	523.3	89.0	0.0463	0.2022	0.2012	2.042	0.002	0.00340	263.0	3.443	0.8701	0.249	1.49	249.8	0.2993	4.5	0.05562	102.0	2669	0.00370	3.078	3936
141	1.309	0.02072	0.0186	0.014	0.0016	26	0.863	0.01394	523.3	88.8	0.0462	0.2018	0.2012	2.038	0.002	0.00340	262.9	3.435	0.8683	0.249	1.49	249.4	0.2987	4.5	0.05550	101.8	2668	0.00370	3.072	3934
142	1.309	0.02072	0.0186	0.014	0.0016	26	0.863	0.01393	523.4	88.7	0.0461	0.2017	0.2012	2.035	0.002	0.00340	263.0	3.431	0.8674	0.249	1.49	249.2	0.2985	4.5	0.05542	101.6	2669	0.00369	3.070	3934
143	1.309	0.02070	0.0186	0.014	0.0016	26	0.862	0.01391	523.5	88.5	0.0460	0.2014	0.2012	2.030	0.002	0.00339	262.8	3.424	0.8657	0.249	1.49	248.8	0.2979	4.5	0.05530	101.4	2667	0.00368	3.064	3932
144	1.309	0.02067	0.0185	0.014	0.0016	26	0.861	0.01387	523.6	88.3	0.0459	0.2010	0.2012	2.025	0.002	0.00339	262.7	3.415	0.8637	0.248	1.49	248.3	0.2973	4.5	0.05516	101.1	2666	0.00367	3.058	3929
145	1.309	0.02065	0.0185	0.014	0.0016	26	0.860	0.01384	523.7	88.0	0.0458	0.2006	0.2012	2.020	0.002	0.00339	262.5	3.406	0.8616	0.248	1.49	247.8	0.2967	4.5	0.05501	100.9	2665	0.00366	3.051	3927
146	1.309	0.02063	0.0185	0.014	0.0016	26	0.859	0.01382	523.8	87.8	0.0457	0.2003	0.2012	2.015	0.002	0.00339	262.5	3.398	0.8598	0.248	1.49	247.4	0.2961	4.5	0.05488	100.6	2664	0.00365	3.045	3926
147	1.309	0.02064	0.0186	0.014	0.0016	26	0.859	0.01380	523.8	87.7	0.0456	0.2002	0.2012	2.012	0.002	0.00339	262.6	3.394	0.8589	0.247	1.49	247.2	0.2959	4.5	0.05481	100.5	2665	0.00365	3.043	3926
148	1.309	0.02062	0.0186	0.014	0.0016	26	0.858	0.01377	523.9	87.5	0.0455	0.1998	0.2012	2.007	0.002	0.00338	262.5	3.384	0.8569	0.247	1.49	246.8	0.2952	4.5	0.05466	100.2	2664	0.00364	3.037	3924
149	1.309	0.02059	0.0186	0.014	0.0016	26	0.857	0.01374	524.0	87.2	0.0454	0.1995	0.2012	2.001	0.002	0.00338	262.4	3.375	0.8548	0.247	1.49	246.3	0.2946	4.5	0.05451	100.0	2663	0.00363	3.030	3922
150	1.309	0.02057	0.0186	0.014	0.0016	26	0.856	0.01371	524.1	87.0	0.0453	0.1991	0.2012	1.996	0.002	0.00338	262.4	3.366	0.8527	0.246	1.49	245.8	0.2940	4.5	0.05436	99.7	2662	0.00362	3.024	3920
151	1.309	0.02056	0.0186	0.014	0.0016	26	0.856	0.01369	524.2	86.8	0.0452	0.1988	0.2012	1.991	0.002	0.00338	262.4	3.359	0.8510	0.246	1.49	245.5	0.2935	4.5	0.05424	99.4	2661	0.00361	3.018	3919
152	1.309	0.02057	0.0186	0.014	0.0016	26	0.856	0.01368	524.2	86.7	0.0451	0.1987	0.2012	1.989	0.002	0.00338	262.6	3.355	0.8503	0.246	1.49	245.3	0.2933	4.5	0.05417	99.3	2662	0.00361	3.016	3919
153	1.309	0.02055	0.0186	0.014	0.0016	26	0.855	0.01365	524.3	86.5	0.0450	0.1984	0.2012	1.984	0.002	0.00338	262.5	3.346	0.8484	0.246	1.49	244.9	0.2927	4.5	0.054					

Table 5. Tailings Seepage Concentrations - Alternative 4

Years since Mine Start	Al	Sb	As	Ba	Be	HCO3	B	Cd	Ca	Cl	Cr	Co	Cu	F	Fe	Pb	Mg	Mn	Mo	Ni	NO3-N	K	Se	Si	Ag	Na	SO4	Tl	Zn	TDS
	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	
199	1.309	0.02055	0.0192	0.014	0.0016	26	0.853	0.01303	526.0	80.9	0.0421	0.1924	0.2012	1.855	0.002	0.00340	268.9	3.135	0.8044	0.241	1.49	236.8	0.2805	4.5	0.05057	92.7	2675	0.00337	2.886	3918
200	1.309	0.02056	0.0193	0.014	0.0016	26	0.854	0.01302	526.0	80.8	0.0420	0.1923	0.2012	1.854	0.002	0.00340	269.1	3.132	0.8038	0.241	1.49	236.8	0.2804	4.5	0.05052	92.6	2675	0.00336	2.884	3919
201	1.309	0.02057	0.0193	0.014	0.0016	26	0.854	0.01301	526.0	80.7	0.0420	0.1922	0.2012	1.852	0.002	0.00341	269.3	3.129	0.8032	0.241	1.49	236.7	0.2802	4.5	0.05047	92.5	2676	0.00336	2.883	3919
202	1.309	0.02058	0.0193	0.014	0.0016	26	0.855	0.01302	526.0	80.7	0.0420	0.1923	0.2012	1.852	0.002	0.00341	269.6	3.129	0.8034	0.241	1.49	236.8	0.2803	4.5	0.05048	92.5	2677	0.00336	2.884	3921
203	1.309	0.02059	0.0193	0.014	0.0016	26	0.855	0.01301	526.0	80.7	0.0420	0.1923	0.2012	1.850	0.002	0.00341	269.8	3.127	0.8030	0.241	1.49	236.7	0.2802	4.5	0.05044	92.4	2678	0.00336	2.883	3922
204	1.309	0.02060	0.0193	0.014	0.0016	26	0.855	0.01301	526.0	80.6	0.0419	0.1923	0.2012	1.849	0.002	0.00341	269.9	3.124	0.8025	0.241	1.49	236.7	0.2801	4.5	0.05040	92.4	2678	0.00335	2.882	3922
205	1.309	0.02060	0.0193	0.014	0.0016	26	0.855	0.01300	526.0	80.6	0.0419	0.1922	0.2012	1.848	0.002	0.00341	270.1	3.122	0.8021	0.241	1.49	236.6	0.2800	4.5	0.05036	92.3	2679	0.00335	2.880	3923
206	1.309	0.02061	0.0194	0.014	0.0016	26	0.856	0.01300	526.0	80.5	0.0419	0.1923	0.2012	1.847	0.002	0.00342	270.3	3.121	0.8021	0.241	1.49	236.7	0.2800	4.5	0.05035	92.3	2680	0.00335	2.881	3924
207	1.309	0.02063	0.0194	0.014	0.0016	26	0.856	0.01300	526.0	80.5	0.0419	0.1923	0.2012	1.846	0.002	0.00342	270.6	3.120	0.8018	0.241	1.49	236.7	0.2800	4.5	0.05032	92.2	2681	0.00335	2.880	3925
208	1.309	0.02064	0.0194	0.014	0.0016	26	0.857	0.01300	526.0	80.5	0.0419	0.1923	0.2012	1.846	0.002	0.00342	270.8	3.119	0.8017	0.242	1.49	236.7	0.2800	4.5	0.05031	92.2	2682	0.00335	2.880	3926
209	1.309	0.02064	0.0194	0.014	0.0016	26	0.857	0.01299	526.0	80.4	0.0418	0.1923	0.2012	1.844	0.002	0.00342	271.0	3.116	0.8011	0.242	1.49	236.6	0.2798	4.5	0.05026	92.1	2682	0.00334	2.879	3926
210	1.309	0.02065	0.0194	0.014	0.0016	26	0.857	0.01299	526.0	80.3	0.0418	0.1922	0.2012	1.842	0.002	0.00342	271.2	3.114	0.8008	0.242	1.49	236.6	0.2798	4.5	0.05022	92.0	2683	0.00334	2.878	3927
211	1.309	0.02066	0.0195	0.014	0.0016	26	0.858	0.01299	526.0	80.3	0.0418	0.1923	0.2012	1.842	0.002	0.00343	271.4	3.113	0.8008	0.242	1.49	236.6	0.2798	4.5	0.05022	92.0	2684	0.00334	2.878	3928
212	1.309	0.02068	0.0195	0.014	0.0016	26	0.858	0.01299	526.0	80.3	0.0418	0.1923	0.2012	1.841	0.002	0.00343	271.7	3.112	0.8006	0.242	1.49	236.7	0.2798	4.5	0.05020	92.0	2685	0.00334	2.878	3930
213	1.309	0.02069	0.0195	0.014	0.0016	26	0.859	0.01299	526.0	80.3	0.0418	0.1924	0.2012	1.841	0.002	0.00343	271.9	3.111	0.8006	0.242	1.49	236.7	0.2798	4.5	0.05019	92.0	2686	0.00334	2.879	3931
214	1.309	0.02069	0.0195	0.014	0.0016	26	0.859	0.01298	526.0	80.2	0.0417	0.1923	0.2012	1.839	0.002	0.00343	272.1	3.109	0.8000	0.242	1.49	236.6	0.2797	4.5	0.05014	91.9	2686	0.00334	2.877	3931
215	1.309	0.02070	0.0195	0.014	0.0016	26	0.859	0.01298	526.0	80.2	0.0417	0.1923	0.2012	1.839	0.002	0.00343	272.3	3.108	0.8000	0.242	1.49	236.7	0.2797	4.5	0.05014	91.9	2687	0.00334	2.877	3932
216	1.309	0.02071	0.0195	0.014	0.0016	26	0.860	0.01298	526.0	80.2	0.0417	0.1924	0.2012	1.838	0.002	0.00344	272.5	3.107	0.7999	0.242	1.49	236.7	0.2797	4.5	0.05012	91.8	2688	0.00334	2.877	3933
217	1.309	0.02073	0.0196	0.014	0.0016	26	0.860	0.01298	526.0	80.2	0.0417	0.1924	0.2012	1.838	0.002	0.00344	272.8	3.107	0.8000	0.242	1.49	236.8	0.2798	4.5	0.05011	91.8	2689	0.00333	2.878	3935
218	1.309	0.02074	0.0196	0.014	0.0016	26	0.861	0.01298	526.0	80.1	0.0417	0.1925	0.2012	1.837	0.002	0.00344	273.0	3.106	0.7998	0.242	1.49	236.8	0.2797	4.5	0.05009	91.8	2690	0.00333	2.878	3936
219	1.309	0.02075	0.0196	0.014	0.0016	26	0.861	0.01297	526.0	80.1	0.0416	0.1924	0.2012	1.836	0.002	0.00344	273.2	3.103	0.7993	0.242	1.49	236.7	0.2796	4.5	0.0					

Table 6. Model Results at Queen Creek 3 Aquifer Subdomain - Alternative 4

Table 6. Model Results at Queen Creek 3 Aquifer Subdomain - Alternative 4

Years since Mine Start	Al	Sb	As	Ba	Be	HCO3	B	Cd	Ca	Cl	Cr	Co	Cu	F	Fe	Pb	Mg	Mn	Mo	Ni	NO3-N	K	Se	Si	Ag	Na	SO4	Tl	Zn	TDS
	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	
68	0.014	0.00023	0.00020	0.00014	0.00002	0	0.010	0.00016	5.4	1.1	0.0006	0.0024	0.0021	0.02	0.00002	0.00004	2.9	0.041	0.0103	0.0029	0.02	2.9	0.0035	0.0	0.00067	1.2	29	0.00004	0.036	43
69	0.014	0.00024	0.00020	0.00014	0.00002	0	0.010	0.00017	5.4	1.1	0.0006	0.0024	0.0021	0.02	0.00002	0.00004	2.9	0.042	0.0104	0.0029	0.02	2.9	0.0035	0.0	0.00067	1.2	29	0.00004	0.036	43
70	0.014	0.00024	0.00020	0.00015	0.00002	0	0.010	0.00017	5.4	1.1	0.0006	0.0024	0.0021	0.02	0.00002	0.00004	2.9	0.042	0.0105	0.0029	0.02	3.0	0.0036	0.0	0.00068	1.2	29	0.00005	0.037	43
71	0.014	0.00024	0.00021	0.00015	0.00002	0	0.010	0.00017	5.5	1.1	0.0006	0.0024	0.0021	0.02	0.00002	0.00004	2.9	0.042	0.0105	0.0029	0.02	3.0	0.0036	0.0	0.00068	1.2	29	0.00005	0.037	43
72	0.014	0.00024	0.00021	0.00015	0.00002	0	0.010	0.00017	5.5	1.1	0.0006	0.0024	0.0021	0.03	0.00002	0.00004	3.0	0.042	0.0105	0.0029	0.02	3.0	0.0036	0.0	0.00068	1.3	29	0.00005	0.037	44
73	0.014	0.00024	0.00021	0.00015	0.00002	0	0.010	0.00017	5.5	1.1	0.0006	0.0024	0.0021	0.03	0.00002	0.00004	3.0	0.042	0.0106	0.0029	0.02	3.0	0.0036	0.0	0.00068	1.3	29	0.00005	0.037	44
74	0.014	0.00024	0.00021	0.00015	0.00002	0	0.010	0.00017	5.5	1.1	0.0006	0.0024	0.0022	0.03	0.00002	0.00004	3.0	0.042	0.0106	0.0030	0.02	3.0	0.0036	0.0	0.00069	1.3	30	0.00005	0.037	44
75	0.014	0.00024	0.00021	0.00015	0.00002	0	0.010	0.00017	5.6	1.1	0.0006	0.0024	0.0022	0.03	0.00002	0.00004	3.0	0.043	0.0107	0.0030	0.02	3.0	0.0036	0.0	0.00069	1.3	30	0.00005	0.037	44
76	0.014	0.00024	0.00021	0.00015	0.00002	0	0.010	0.00017	5.6	1.1	0.0006	0.0024	0.0022	0.03	0.00002	0.00004	3.0	0.043	0.0107	0.0030	0.02	3.0	0.0037	0.0	0.00069	1.3	30	0.00005	0.038	44
77	0.014	0.00025	0.00021	0.00015	0.00002	0	0.010	0.00017	5.6	1.1	0.0006	0.0025	0.0022	0.03	0.00002	0.00004	3.1	0.043	0.0108	0.0030	0.02	3.1	0.0037	0.0	0.00070	1.3	30	0.00005	0.038	45
78	0.014	0.00025	0.00021	0.00015	0.00002	0	0.010	0.00017	5.6	1.1	0.0006	0.0025	0.0022	0.03	0.00002	0.00004	3.1	0.043	0.0108	0.0030	0.02	3.1	0.0037	0.0	0.00070	1.3	30	0.00005	0.038	45
79	0.014	0.00025	0.00021	0.00015	0.00002	0	0.010	0.00017	5.7	1.1	0.0006	0.0025	0.0022	0.03	0.00002	0.00004	3.1	0.043	0.0109	0.0030	0.02	3.1	0.0037	0.0	0.00070	1.3	30	0.00005	0.038	45
80	0.014	0.00025	0.00022	0.00015	0.00002	0	0.010	0.00017	5.7	1.1	0.0006	0.0025	0.0022	0.03	0.00002	0.00004	3.1	0.044	0.0109	0.0030	0.02	3.1	0.0037	0.0	0.00071	1.3	31	0.00005	0.038	45
81	0.015	0.00025	0.00022	0.00015	0.00002	0	0.010	0.00018	5.7	1.1	0.0006	0.0025	0.0022	0.03	0.00002	0.00004	3.1	0.044	0.0110	0.0031	0.02	3.1	0.0037	0.0	0.00071	1.3	31	0.00005	0.038	46
82	0.015	0.00025	0.00022	0.00015	0.00002	0	0.010	0.00018	5.8	1.1	0.0006	0.0025	0.0022	0.03	0.00002	0.00004	3.1	0.044	0.0110	0.0031	0.02	3.1	0.0038	0.0	0.00071	1.3	31	0.00005	0.039	46
83	0.015	0.00025	0.00022	0.00016	0.00002	0	0.011	0.00018	5.8	1.1	0.0006	0.0025	0.0023	0.03	0.00002	0.00004	3.1	0.044	0.0110	0.0031	0.02	3.1	0.0038	0.1	0.00071	1.3	31	0.00005	0.039	46
84	0.015	0.00025	0.00022	0.00016	0.00002	0	0.011	0.00018	5.8	1.1	0.0006	0.0025	0.0023	0.03	0.00002	0.00004	3.1	0.044	0.0111	0.0031	0.02	3.1	0.0038	0.1	0.00071	1.3	31	0.00005	0.039	46
85	0.015	0.00025	0.00022	0.00016	0.00002	0	0.011	0.00018	5.8	1.1	0.0006	0.0025	0.0023	0.03	0.00002	0.00004	3.2	0.044	0.0111	0.0031	0.02	3.1	0.0038	0.1	0.00072	1.3	31	0.00005	0.039	46
86	0.015	0.00026	0.00022	0.00016	0.00002	0	0.011	0.00018	5.9	1.2	0.0006	0.0026	0.0023	0.03	0.00002	0.00004	3.2	0.044	0.0112	0.0031	0.02	3.2	0.0038	0.1	0.00072	1.3	31	0.00005	0.039	47
87	0.015	0.00026	0.00022	0.00016	0.00002	0	0.011	0.00018	5.9	1.2	0.0006	0.0026	0.0023	0.03	0.00002	0.00004	3.2	0.045	0.0112	0.0031	0.02	3.2	0.0038	0.1	0.00072	1.3	32	0.00005	0.039	47
88	0.015	0.00026	0.00022	0.00016	0.00002	0	0.011	0.00018	5.9	1.2	0.0006	0.0026	0.0023	0.03	0.00002	0.00004	3.2	0.045	0.0112	0.0031	0.02	3.2	0.0038	0.1	0.00073	1.3	32	0.00005	0.039	47
89	0.015	0.00026	0.00023	0.00016	0.00002	0	0.011	0.00018	6.0	1.																				

Table 6. Model Results at Queen Creek 3 Aquifer Subdomain - Alternative 4

Years since Mine Start	Al	Sb	As	Ba	Be	HCO3	B	Cd	Ca	Cl	Cr	Co	Cu	F	Fe	Pb	Mg	Mn	Mo	Ni	NO3-N	K	Se	Si	Ag	Na	SO4	Tl	Zn	TDS
	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	
135	0.018	0.00029	0.00026	0.00020	0.00002	0	0.012	0.00020	7.4	1.3	0.0007	0.0029	0.0028	0.03	0.00002	0.00005	3.7	0.049	0.0124	0.0036	0.02	3.6	0.0043	0.1	0.00080	1.5	38	0.00005	0.044	56
136	0.019	0.00030	0.00026	0.00020	0.00002	0	0.012	0.00020	7.4	1.3	0.0007	0.0029	0.0028	0.03	0.00002	0.00005	3.7	0.049	0.0125	0.0036	0.02	3.6	0.0043	0.1	0.00080	1.5	38	0.00005	0.044	56
137	0.019	0.00030	0.00026	0.00020	0.00002	0	0.012	0.00020	7.4	1.3	0.0007	0.0029	0.0029	0.03	0.00002	0.00005	3.8	0.049	0.0125	0.0036	0.02	3.6	0.0043	0.1	0.00080	1.5	38	0.00005	0.044	56
138	0.019	0.00030	0.00027	0.00020	0.00002	0	0.012	0.00020	7.5	1.3	0.0007	0.0029	0.0029	0.03	0.00003	0.00005	3.8	0.050	0.0125	0.0036	0.02	3.6	0.0043	0.1	0.00080	1.5	38	0.00005	0.044	56
139	0.019	0.00030	0.00027	0.00020	0.00002	0	0.012	0.00020	7.5	1.3	0.0007	0.0029	0.0029	0.03	0.00003	0.00005	3.8	0.050	0.0126	0.0036	0.02	3.6	0.0043	0.1	0.00080	1.5	38	0.00005	0.044	57
140	0.019	0.00030	0.00027	0.00020	0.00002	0	0.012	0.00020	7.5	1.3	0.0007	0.0029	0.0029	0.03	0.00003	0.00005	3.8	0.050	0.0126	0.0036	0.02	3.6	0.0043	0.1	0.00080	1.5	38	0.00005	0.044	57
141	0.019	0.00030	0.00027	0.00020	0.00002	0	0.012	0.00020	7.6	1.3	0.0007	0.0029	0.0029	0.03	0.00003	0.00005	3.8	0.050	0.0126	0.0036	0.02	3.6	0.0043	0.1	0.00080	1.5	39	0.00005	0.045	57
142	0.019	0.00030	0.00027	0.00020	0.00002	0	0.013	0.00020	7.6	1.3	0.0007	0.0029	0.0029	0.03	0.00003	0.00005	3.8	0.050	0.0126	0.0036	0.02	3.6	0.0043	0.1	0.00081	1.5	39	0.00005	0.045	57
143	0.019	0.00030	0.00027	0.00020	0.00002	0	0.013	0.00020	7.6	1.3	0.0007	0.0029	0.0029	0.03	0.00003	0.00005	3.8	0.050	0.0126	0.0036	0.02	3.6	0.0043	0.1	0.00081	1.5	39	0.00005	0.045	57
144	0.019	0.00030	0.00027	0.00020	0.00002	0	0.013	0.00020	7.7	1.3	0.0007	0.0029	0.0029	0.03	0.00003	0.00005	3.8	0.050	0.0127	0.0036	0.02	3.6	0.0044	0.1	0.00081	1.5	39	0.00005	0.045	58
145	0.019	0.00030	0.00027	0.00020	0.00002	0	0.013	0.00020	7.7	1.3	0.0007	0.0030	0.0030	0.03	0.00003	0.00005	3.9	0.050	0.0127	0.0036	0.02	3.6	0.0044	0.1	0.00081	1.5	39	0.00005	0.045	58
146	0.019	0.00030	0.00027	0.00020	0.00002	0	0.013	0.00020	7.7	1.3	0.0007	0.0030	0.0030	0.03	0.00003	0.00005	3.9	0.050	0.0127	0.0037	0.02	3.7	0.0044	0.1	0.00081	1.5	39	0.00005	0.045	58
147	0.019	0.00030	0.00027	0.00020	0.00002	0	0.013	0.00020	7.7	1.3	0.0007	0.0030	0.0030	0.03	0.00003	0.00005	3.9	0.050	0.0127	0.0037	0.02	3.7	0.0044	0.1	0.00081	1.5	39	0.00005	0.045	58
148	0.019	0.00031	0.00027	0.00021	0.00002	0	0.013	0.00020	7.7	1.3	0.0007	0.0030	0.0030	0.03	0.00003	0.00005	3.9	0.050	0.0127	0.0037	0.02	3.7	0.0044	0.1	0.00081	1.5	39	0.00005	0.045	58
149	0.019	0.00031	0.00028	0.00021	0.00002	0	0.013	0.00020	7.8	1.3	0.0007	0.0030	0.0030	0.03	0.00003	0.00005	3.9	0.050	0.0127	0.0037	0.02	3.7	0.0044	0.1	0.00081	1.5	39	0.00005	0.045	58
150	0.019	0.00030	0.00027	0.00020	0.00002	0	0.013	0.00020	7.7	1.3	0.0007	0.0029	0.0029	0.03	0.00003	0.00005	3.8	0.049	0.0125	0.0036	0.02	3.6	0.0043	0.1	0.00080	1.5	39	0.00005	0.044	57
151	0.019	0.00031	0.00028	0.00021	0.00002	0	0.013	0.00020	7.8	1.3	0.0007	0.0030	0.0030	0.03	0.00003	0.00005	3.9	0.050	0.0127	0.0037	0.02	3.6	0.0044	0.1	0.00081	1.5	40	0.00005	0.045	58
152	0.020	0.00031	0.00028	0.00021	0.00002	0	0.013	0.00020	7.8	1.3	0.0007	0.0030	0.0030	0.03	0.00003	0.00005	3.9	0.050	0.0127	0.0037	0.02	3.7	0.0044	0.1	0.00081	1.5	40	0.00005	0.045	58
153	0.020	0.00031	0.00028	0.00021	0.00002	0	0.013	0.00020	7.8	1.3	0.0007	0.0030	0.0030	0.03	0.00003	0.00005	3.9	0.050	0.0127	0.0037	0.02	3.7	0.0044	0.1	0.00081	1.5	40	0.00005	0.045	58
154	0.020	0.00031	0.00028	0.00021	0.00002	0	0.013	0.00020	7.8	1.3	0.0007	0.0030	0.0030	0.03	0.00003	0.00005	3.9	0.050	0.0127	0.0037	0.02	3.7	0.0044	0.1	0.00081	1.5	40	0.00005	0.045	59
155	0.020	0.00031	0.00028	0.00021	0.00002	0	0.013	0.00020	7.9	1.3	0.0007	0.0030	0.0030	0.03	0.00003	0.00005	3.9	0.050	0.0127	0.0037	0.02	3.7	0.0044	0.1	0.00081	1.5	40	0.00005	0.045	59
156	0.020	0.00031	0.00028	0.00021	0.00002	0	0.013																							

Table 6. Model Results at Queen Creek 3 Aquifer Subdomain - Alternative 4

Minimum	0.000	0.00000	0.00000	0.00000	0.00000	0.00000	0	0.000	0.00000	0.0	0.0	0.0000	0.0000	0.0000	0.0000	0.00000	0.00000	0.0	0.000	0.0000	0.0000	0.0000	0.0000	0.0	0.00000	0.00000	0.0000	0	0.00000	0.0000	0.0000	0
Maximum	0.023	0.00037	0.00035	0.00024	0.00003	0	0.015	0.00023	9.2	1.4	0.0007	0.0034	0.0035	0.03	0.00003	0.00006	4.9	0.054	0.0140	0.0043	0.03	4.2	0.0049	0.1	0.00087	1.6	47	0.00006	0.051	69		
Average	0.015	0.00024	0.00022	0.00016	0.00002	0	0.010	0.00016	6.0	1.0	0.0005	0.0024	0.0022	0.02	0.00002	0.00004	3.1	0.040	0.0101	0.0020	0.02	3.0	0.0035	0.1	0.00064	1.2	31	0.00004	0.026	46		

Aquifer WQ Standard = 0.006 0.05 2 0.004 0.005 0.1 4.0 0.05 0.1 10 0.05 0.002

Notes:-

1. Model results do not include background concentrations and assume no mass flux from recharge or natural groundwater sources
 2. Aquifer WQ Standard = Arizona Department of Environmental Quality Numeric Aquifer Water Quality Standards (Arizona Administrative Code - Title 18, Ch. 11, Art. 4, Sup. 16-4, 2016)
 3. Values in bold italic indicate that concentration is above water quality standard
 4. mg/L = milligrams per liter

Table 7. Model Results at Whitlow Ranch Dam - Alternative 4

Table 7. Model Results at Whitlow Ranch Dam - Alternative 4

Years since Mine Start	Al mg/L	Sb mg/L	As mg/L	Ba mg/L	Be mg/L	HCO3 mg/L	B mg/L	Cd mg/L	Ca mg/L	Cl mg/L	Cr mg/L	Cu mg/L	F mg/L	Fe mg/L	Pb mg/L	Mg mg/L	Mn mg/L	Mo mg/L	Ni mg/L	NO3-N mg/L	K mg/L	Se mg/L	Si mg/L	Ag mg/L	Na mg/L	SO4 mg/L	Tl mg/L	Zn mg/L	TDS mg/L	
69	0.007	0.00012	0.0001	0.00007	0.00001	0.141	0.005	0.00009	2.8	0.6	0.0003	0.0012	0.0011	0.013	0.00001	0.00002	1.5	0.021	0.0054	0.0015	0.01	1.5	0.0018	0.024	0.00035	0.6	15	0.00002	0.0187	22
70	0.007	0.00012	0.0001	0.00008	0.00001	0.142	0.005	0.00009	2.8	0.6	0.0003	0.0012	0.0011	0.013	0.00001	0.00002	1.5	0.022	0.0054	0.0015	0.01	1.5	0.0018	0.024	0.00035	0.6	15	0.00002	0.0189	22
71	0.007	0.00012	0.0001	0.00008	0.00001	0.143	0.005	0.00009	2.8	0.6	0.0003	0.0012	0.0011	0.013	0.00001	0.00002	1.5	0.022	0.0054	0.0015	0.01	1.5	0.0018	0.024	0.00035	0.6	15	0.00002	0.0190	22
72	0.007	0.00012	0.0001	0.00008	0.00001	0.144	0.005	0.00009	2.8	0.6	0.0003	0.0012	0.0011	0.013	0.00001	0.00002	1.5	0.022	0.0054	0.0015	0.01	1.5	0.0019	0.024	0.00035	0.6	15	0.00002	0.0191	22
73	0.007	0.00012	0.0001	0.00008	0.00001	0.144	0.005	0.00009	2.8	0.6	0.0003	0.0012	0.0011	0.013	0.00001	0.00002	1.5	0.022	0.0055	0.0015	0.01	1.5	0.0019	0.025	0.00035	0.6	15	0.00002	0.0191	23
74	0.007	0.00012	0.0001	0.00008	0.00001	0.145	0.005	0.00009	2.8	0.6	0.0003	0.0012	0.0011	0.013	0.00001	0.00002	1.5	0.022	0.0055	0.0015	0.01	1.5	0.0019	0.025	0.00035	0.6	15	0.00002	0.0192	23
75	0.007	0.00013	0.0001	0.00008	0.00001	0.146	0.005	0.00009	2.9	0.6	0.0003	0.0013	0.0011	0.013	0.00001	0.00002	1.6	0.022	0.0055	0.0015	0.01	1.6	0.0019	0.025	0.00036	0.7	15	0.00002	0.0193	23
76	0.007	0.00013	0.0001	0.00008	0.00001	0.147	0.005	0.00009	2.9	0.6	0.0003	0.0013	0.0011	0.013	0.00001	0.00002	1.6	0.022	0.0055	0.0015	0.01	1.6	0.0019	0.025	0.00036	0.7	15	0.00002	0.0194	23
77	0.007	0.00013	0.0001	0.00008	0.00001	0.147	0.005	0.00009	2.9	0.6	0.0003	0.0013	0.0011	0.013	0.00001	0.00002	1.6	0.022	0.0056	0.0015	0.01	1.6	0.0019	0.025	0.00036	0.7	16	0.00002	0.0195	23
78	0.007	0.00013	0.0001	0.00008	0.00001	0.148	0.005	0.00009	2.9	0.6	0.0003	0.0013	0.0011	0.013	0.00001	0.00002	1.6	0.022	0.0056	0.0016	0.01	1.6	0.0019	0.025	0.00036	0.7	16	0.00002	0.0196	23
79	0.007	0.00013	0.0001	0.00008	0.00001	0.149	0.005	0.00009	2.9	0.6	0.0003	0.0013	0.0011	0.013	0.00001	0.00002	1.6	0.022	0.0056	0.0016	0.01	1.6	0.0019	0.025	0.00036	0.7	16	0.00002	0.0197	23
80	0.007	0.00013	0.0001	0.00008	0.00001	0.150	0.005	0.00009	2.9	0.6	0.0003	0.0013	0.0011	0.013	0.00001	0.00002	1.6	0.022	0.0056	0.0016	0.01	1.6	0.0019	0.026	0.00036	0.7	16	0.00002	0.0197	23
81	0.007	0.00013	0.0001	0.00008	0.00001	0.151	0.005	0.00009	3.0	0.6	0.0003	0.0013	0.0012	0.013	0.00001	0.00002	1.6	0.023	0.0057	0.0016	0.01	1.6	0.0019	0.026	0.00037	0.7	16	0.00002	0.0199	24
82	0.008	0.00013	0.0001	0.00008	0.00001	0.151	0.005	0.00009	3.0	0.6	0.0003	0.0013	0.0012	0.013	0.00001	0.00002	1.6	0.023	0.0057	0.0016	0.01	1.6	0.0019	0.026	0.00037	0.7	16	0.00002	0.0199	24
83	0.008	0.00013	0.0001	0.00008	0.00001	0.152	0.005	0.00009	3.0	0.6	0.0003	0.0013	0.0012	0.014	0.00001	0.00002	1.6	0.023	0.0057	0.0016	0.01	1.6	0.0019	0.026	0.00037	0.7	16	0.00002	0.0200	24
84	0.008	0.00013	0.0001	0.00008	0.00001	0.153	0.005	0.00009	3.0	0.6	0.0003	0.0013	0.0012	0.014	0.00001	0.00002	1.6	0.023	0.0057	0.0016	0.01	1.6	0.0020	0.026	0.00037	0.7	16	0.00002	0.0201	24
85	0.008	0.00013	0.0001	0.00008	0.00001	0.153	0.005	0.00009	3.0	0.6	0.0003	0.0013	0.0012	0.014	0.00001	0.00002	1.6	0.023	0.0057	0.0016	0.01	1.6	0.0020	0.026	0.00037	0.7	16	0.00002	0.0201	24
86	0.008	0.00013	0.0001	0.00008	0.00001	0.154	0.005	0.00009	3.0	0.6	0.0003	0.0013	0.0012	0.014	0.00001	0.00002	1.6	0.023	0.0058	0.0016	0.01	1.6	0.0020	0.026	0.00037	0.7	16	0.00002	0.0202	24
87	0.008	0.00013	0.0001	0.00008	0.00001	0.155	0.006	0.00009	3.0	0.6	0.0003	0.0013	0.0012	0.014	0.00001	0.00002	1.6	0.023	0.0058	0.0016	0.01	1.6	0.0020	0.026	0.00037	0.7	16	0.00002	0.0203	24
88	0.008	0.00013	0.0001	0.00008	0.00001	0.156	0.006	0.00009	3.1	0.6	0.0003	0.0013	0.0012	0.014	0.00001	0.00002	1.7	0.023	0.0058	0.0016	0.01	1.6	0.0020	0.027	0.00037	0.7	16	0.00002	0.0204	24
89	0.008	0.00013	0.0001	0.00008	0.00001	0.156	0.006	0.00009	3.1	0.6	0.0003	0.0013	0.0012	0.014	0.00001	0.00002	1.7	0.023	0.0058	0.0016	0.01	1.7	0.0020	0.027	0.00038	0.7	16	0.00003	0.0205	24
90	0.008	0.00013	0.0001	0.00008	0.00001	0.157	0.006	0.00009	3.1	0.6	0.0003	0.0013	0.0012	0.014	0.00001	0.00002</td														

Table 7. Model Results at Whitlow Ranch Dam - Alternative 4

Table 7. Model Results at Whitlow Ranch Dam - Alternative 4

Minimum	0.000	0.00000	0.0000	0.00000	0.00000	0.000	0.000	0.00000	0.0	0.0	0.0000	0.0000	0.0000	0.00000	0.00000	0.0	0.000	0.0000	0.0000	0.0000	0.00000	0.0000	0.0	0.00000	0.0000	0	
Maximum	0.012	0.00019	0.0002	0.00013	0.00001	0.236	0.008	0.00012	4.8	0.7	0.0004	0.0018	0.0018	0.017	0.00002	0.00003	2.5	0.028	0.0073	0.0022	0.01	2.2	0.0026	0.041	0.00046	0.8	25
Average	0.008	0.00013	0.0001	0.00008	0.00001	0.155	0.005	0.00008	3.1	0.5	0.0003	0.0012	0.0012	0.012	0.00001	0.00002	1.6	0.020	0.0052	0.0015	0.01	1.5	0.0018	0.027	0.00033	0.6	16

Surface WQ Standard = 0.03000 0.15000 0.00512^a 0.02335^a 1.000 0.00833^a 0.13433^a 0.0020 0.15000 0.3031^b

Notes:

1. Model results do not include background concentrations and assume no mass flux from recharge or natural groundwater sources
 2. Surface WQ Standard = Arizona Department of Environmental Quality Water Quality Standard for "Aquatic and wildlife warm" (A&ww) water with chronic exposure (Arizona Administrative Code - Title 18, Ch. 11, Sup. 16-4, 2016)
 3. Values in bold italic indicate that concentration is above water quality standard
 4. mg/L = milligrams per liter

Table 8. Predicted Total Concentrations at Queen Creek 3 Aquifer Subdomain - Alternative 4

Table 8. Predicted Total Concentrations at Queen Creek 3 Aquifer Subdomain - Alternative 4

Years since Mine Start	Al	Sb	As	Ba	Be	HCO3	B	Cd	Ca	Cl	Cr	Co	Cu	F	Fe	Pb	Mg	Mn	Mo	Ni	NO3-N	K	Se	Si	Ag	Na	SO4	Tl	Zn	TDS
	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	
68	0.054	0.00044	0.0015	0.026	0.0010	340	0.079	0.00020	106.9	30.8	0.0025	0.0037	0.0028	0.55	0.045	0.00010	28.7	0.046	0.0133	0.0056	0.40	6.4	0.0044	42.8	0.00070	54.0	202	0.00007	0.041	632
69	0.054	0.00045	0.0015	0.026	0.0010	340	0.079	0.00020	106.9	30.8	0.0025	0.0037	0.0029	0.55	0.045	0.00010	28.8	0.046	0.0134	0.0056	0.40	6.4	0.0044	42.8	0.00071	54.0	202	0.00007	0.041	632
70	0.054	0.00045	0.0015	0.026	0.0010	340	0.079	0.00020	106.9	30.8	0.0025	0.0037	0.0029	0.55	0.045	0.00010	28.8	0.047	0.0135	0.0056	0.40	6.4	0.0045	42.8	0.00071	54.0	202	0.00008	0.042	632
71	0.054	0.00045	0.0015	0.026	0.0010	340	0.079	0.00021	107.0	30.8	0.0025	0.0037	0.0029	0.55	0.045	0.00010	28.8	0.047	0.0135	0.0056	0.40	6.4	0.0045	42.8	0.00071	54.0	202	0.00008	0.042	632
72	0.054	0.00045	0.0015	0.026	0.0010	340	0.079	0.00021	107.0	30.8	0.0025	0.0037	0.0029	0.55	0.045	0.00010	28.8	0.047	0.0135	0.0056	0.40	6.4	0.0045	42.8	0.00072	54.1	202	0.00008	0.042	633
73	0.054	0.00045	0.0015	0.026	0.0010	340	0.079	0.00021	107.0	30.8	0.0025	0.0037	0.0029	0.55	0.045	0.00010	28.8	0.047	0.0136	0.0056	0.40	6.4	0.0045	42.8	0.00072	54.1	202	0.00008	0.042	633
74	0.054	0.00045	0.0015	0.026	0.0010	340	0.079	0.00021	107.0	30.8	0.0025	0.0037	0.0029	0.55	0.045	0.00010	28.8	0.047	0.0136	0.0057	0.40	6.4	0.0045	42.8	0.00072	54.1	203	0.00008	0.042	633
75	0.054	0.00045	0.0015	0.026	0.0010	340	0.079	0.00021	107.1	30.8	0.0025	0.0037	0.0029	0.55	0.045	0.00010	28.9	0.048	0.0137	0.0057	0.40	6.5	0.0045	42.8	0.00073	54.1	203	0.00008	0.042	633
76	0.054	0.00045	0.0015	0.026	0.0010	340	0.079	0.00021	107.1	30.8	0.0025	0.0037	0.0029	0.55	0.045	0.00010	28.9	0.048	0.0137	0.0057	0.40	6.5	0.0046	42.8	0.00073	54.1	203	0.00008	0.043	633
77	0.054	0.00046	0.0015	0.026	0.0010	340	0.079	0.00021	107.1	30.8	0.0025	0.0038	0.0030	0.55	0.045	0.00011	28.9	0.048	0.0138	0.0057	0.40	6.5	0.0046	42.8	0.00073	54.1	203	0.00008	0.043	634
78	0.054	0.00046	0.0015	0.026	0.0010	340	0.079	0.00021	107.1	30.8	0.0025	0.0038	0.0030	0.55	0.045	0.00011	28.9	0.048	0.0139	0.0057	0.40	6.5	0.0046	42.8	0.00074	54.1	203	0.00008	0.043	634
79	0.054	0.00046	0.0015	0.026	0.0010	340	0.079	0.00021	107.2	30.8	0.0025	0.0038	0.0030	0.55	0.045	0.00011	28.9	0.048	0.0139	0.0057	0.40	6.5	0.0046	42.8	0.00074	54.1	203	0.00008	0.043	634
80	0.054	0.00046	0.0015	0.026	0.0010	340	0.079	0.00021	107.2	30.8	0.0025	0.0038	0.0030	0.55	0.045	0.00011	28.9	0.049	0.0139	0.0057	0.40	6.5	0.0046	42.8	0.00074	54.1	204	0.00008	0.043	634
81	0.055	0.00046	0.0015	0.026	0.0010	340	0.079	0.00021	107.2	30.8	0.0025	0.0038	0.0030	0.55	0.045	0.00011	29.0	0.049	0.0140	0.0058	0.40	6.5	0.0046	42.8	0.00074	54.1	204	0.00008	0.043	635
82	0.055	0.00046	0.0015	0.026	0.0010	340	0.079	0.00021	107.3	30.8	0.0025	0.0038	0.0030	0.56	0.045	0.00011	29.0	0.049	0.0140	0.0058	0.40	6.5	0.0047	42.8	0.00075	54.1	204	0.00008	0.044	635
83	0.055	0.00046	0.0015	0.026	0.0010	340	0.080	0.00021	107.3	30.8	0.0025	0.0038	0.0030	0.56	0.045	0.00011	29.0	0.049	0.0140	0.0058	0.40	6.6	0.0047	42.9	0.00075	54.1	204	0.00008	0.044	635
84	0.055	0.00046	0.0015	0.026	0.0010	340	0.080	0.00021	107.3	30.8	0.0025	0.0038	0.0030	0.56	0.045	0.00011	29.0	0.049	0.0141	0.0058	0.40	6.6	0.0047	42.9	0.00075	54.1	204	0.00008	0.044	635
85	0.055	0.00046	0.0015	0.026	0.0010	340	0.080	0.00022	107.3	30.8	0.0025	0.0038	0.0030	0.56	0.045	0.00011	29.0	0.049	0.0141	0.0058	0.40	6.6	0.0047	42.9	0.00075	54.1	204	0.00008	0.044	635
86	0.055	0.00047	0.0015	0.026	0.0010	340	0.080	0.00022	107.4	30.9	0.0025	0.0039	0.0031	0.56	0.045	0.00011	29.0	0.050	0.0142	0.0058	0.40	6.6	0.0047	42.9	0.00076	54.1	204	0.00008	0.044	636
87	0.055	0.00047	0.0015	0.026	0.0010	340	0.080	0.00022	107.4	30.9	0.0025	0.0039	0.0031	0.56	0.045	0.00011	29.0	0.050	0.0142	0.0058	0.40	6.6	0.0047	42.9	0.00076	54.1	205	0.00008	0.044	636
88	0.055	0.00047	0.0015	0.026	0.0010	340	0.080	0.00022	107.4	30.9	0.0025	0.0039	0.0031	0.56	0.045	0.00011	29.1	0.050	0.0142	0.0058	0.40	6.6	0.0047	42.9	0.00076	54.1	205	0.00008	0.044	636
89	0.055	0.00047	0																											

Table 8. Predicted Total Concentrations at Queen Creek 3 Aquifer Subdomain - Alternative 4

Years since Mine Start	Al	Sb	As	Ba	Be	HCO3	B	Cd	Ca	Cl	Cr	Co	Cu	F	Fe	Pb	Mg	Mn	Mo	Ni	NO3-N	K	Se	Si	Ag	Na	SO4	Tl	Zn	TDS
	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	
135	0.058	0.00050	0.0015	0.026	0.0010	340	0.081	0.00024	108.9	31.0	0.0026	0.0042	0.0036	0.56	0.045	0.00011	29.6	0.054	0.0154	0.0063	0.40	7.0	0.0052	42.9	0.00083	54.3	211	0.00008	0.049	645
136	0.059	0.00051	0.0015	0.026	0.0010	340	0.081	0.00024	108.9	31.0	0.0026	0.0042	0.0036	0.56	0.045	0.00011	29.6	0.054	0.0155	0.0063	0.40	7.0	0.0052	42.9	0.00083	54.3	211	0.00008	0.049	645
137	0.059	0.00051	0.0015	0.026	0.0010	340	0.081	0.00024	108.9	31.0	0.0026	0.0042	0.0036	0.56	0.045	0.00011	29.6	0.054	0.0155	0.0063	0.40	7.0	0.0052	42.9	0.00083	54.3	211	0.00008	0.049	645
138	0.059	0.00051	0.0015	0.026	0.0010	340	0.081	0.00024	109.0	31.0	0.0026	0.0042	0.0036	0.56	0.045	0.00011	29.6	0.054	0.0155	0.0063	0.40	7.0	0.0052	42.9	0.00084	54.3	211	0.00008	0.049	645
139	0.059	0.00051	0.0015	0.026	0.0010	340	0.081	0.00024	109.0	31.0	0.0026	0.0042	0.0036	0.56	0.045	0.00011	29.6	0.055	0.0156	0.0063	0.40	7.0	0.0052	42.9	0.00084	54.3	211	0.00008	0.049	646
140	0.059	0.00051	0.0015	0.026	0.0010	340	0.081	0.00024	109.0	31.0	0.0026	0.0042	0.0037	0.56	0.045	0.00011	29.6	0.055	0.0156	0.0063	0.40	7.0	0.0052	42.9	0.00084	54.3	211	0.00008	0.049	646
141	0.059	0.00051	0.0015	0.026	0.0010	340	0.081	0.00024	109.1	31.0	0.0026	0.0042	0.0037	0.56	0.045	0.00011	29.7	0.055	0.0156	0.0063	0.40	7.1	0.0052	42.9	0.00084	54.3	212	0.00008	0.050	646
142	0.059	0.00051	0.0015	0.026	0.0010	340	0.082	0.00024	109.1	31.0	0.0026	0.0042	0.0037	0.56	0.045	0.00011	29.7	0.055	0.0156	0.0063	0.40	7.1	0.0052	42.9	0.00084	54.3	212	0.00008	0.050	646
143	0.059	0.00051	0.0016	0.026	0.0010	340	0.082	0.00024	109.1	31.0	0.0026	0.0042	0.0037	0.56	0.045	0.00011	29.7	0.055	0.0156	0.0063	0.40	7.1	0.0052	42.9	0.00084	54.3	212	0.00008	0.050	646
144	0.059	0.00051	0.0016	0.026	0.0010	340	0.082	0.00024	109.2	31.0	0.0026	0.0043	0.0037	0.56	0.045	0.00011	29.7	0.055	0.0157	0.0063	0.40	7.1	0.0053	42.9	0.00085	54.3	212	0.00008	0.050	647
145	0.059	0.00051	0.0016	0.026	0.0010	340	0.082	0.00024	109.2	31.0	0.0026	0.0043	0.0037	0.56	0.045	0.00011	29.7	0.055	0.0157	0.0064	0.40	7.1	0.0053	42.9	0.00085	54.3	212	0.00008	0.050	647
146	0.059	0.00051	0.0016	0.026	0.0010	340	0.082	0.00024	109.2	31.0	0.0026	0.0043	0.0037	0.56	0.045	0.00011	29.7	0.055	0.0157	0.0064	0.40	7.1	0.0053	42.9	0.00085	54.3	212	0.00008	0.050	647
147	0.059	0.00051	0.0016	0.026	0.0010	340	0.082	0.00024	109.2	31.0	0.0026	0.0043	0.0037	0.56	0.045	0.00012	29.7	0.055	0.0157	0.0064	0.40	7.1	0.0053	42.9	0.00085	54.3	212	0.00008	0.050	647
148	0.059	0.00052	0.0016	0.026	0.0010	340	0.082	0.00024	109.2	31.0	0.0026	0.0043	0.0037	0.56	0.045	0.00012	29.7	0.055	0.0157	0.0064	0.40	7.1	0.0053	42.9	0.00085	54.3	212	0.00008	0.050	647
149	0.059	0.00052	0.0016	0.026	0.0010	340	0.082	0.00024	109.3	31.0	0.0026	0.0043	0.0037	0.56	0.045	0.00012	29.7	0.055	0.0157	0.0064	0.40	7.1	0.0053	42.9	0.00085	54.3	212	0.00008	0.050	647
150	0.059	0.00051	0.0016	0.026	0.0010	340	0.082	0.00024	109.2	31.0	0.0026	0.0042	0.0037	0.56	0.045	0.00011	29.7	0.054	0.0155	0.0063	0.40	7.0	0.0052	42.9	0.00083	54.3	212	0.00008	0.049	646
151	0.059	0.00052	0.0016	0.026	0.0010	340	0.082	0.00024	109.3	31.0	0.0026	0.0043	0.0037	0.56	0.045	0.00012	29.7	0.055	0.0157	0.0064	0.40	7.1	0.0053	42.9	0.00084	54.3	213	0.00008	0.050	647
152	0.060	0.00052	0.0016	0.026	0.0010	340	0.082	0.00024	109.3	31.0	0.0026	0.0043	0.0038	0.56	0.045	0.00012	29.8	0.055	0.0157	0.0064	0.40	7.1	0.0053	42.9	0.00084	54.3	213	0.00008	0.050	647
153	0.060	0.00052	0.0016	0.026	0.0010	340	0.082	0.00024	109.3	31.0	0.0026	0.0043	0.0038	0.56	0.045	0.00012	29.8	0.055	0.0157	0.0064	0.40	7.1	0.0053	42.9	0.00084	54.3	213	0.00008	0.050	647
154	0.060	0.00052	0.0016	0.026	0.0010	340	0.082	0.00024	109.3	31.0	0.0026	0.0043	0.0038	0.56	0.045	0.00012	29.8	0.055	0.0157	0.0064	0.40	7.1	0.0053	42.9	0.00084	54.3	213	0.00008	0.050	648
155	0.060	0.00052	0.0016	0.026	0.0010	340	0.082	0.00024	109.4	31.0	0.0026	0.0042	0.0038	0.56	0.045	0.00012	29.8	0.055	0.0157	0.0064	0.40	7.1	0.0053	42.9	0.00084	54.3	213	0.00008	0.050	648

Table 8. Predicted Total Concentrations at Queen Creek 3 Aquifer Subdomain - Alternative 4

Years since Mine Start	Al	Sb	As	Ba	Be	HCO3	B	Cd	Ca	Cl	Cr	Co	Cu	F	Fe	Pb	Mg	Mn	Mo	Ni	NO3-N	K	Se	Si	Ag	Na	SO4	Tl	Zn	TDS
	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	
202	0.061	0.00054	0.0016	0.026	0.0010	340	0.083	0.00025	110.0	31.0	0.0026	0.0044	0.0040	0.56	0.045	0.00012	30.2	0.056	0.0160	0.0066	0.40	7.3	0.0054	42.9	0.00086	54.3	216	0.00008	0.052	653
203	0.061	0.00055	0.0016	0.026	0.0010	340	0.083	0.00025	110.1	31.0	0.0026	0.0044	0.0040	0.56	0.045	0.00012	30.2	0.056	0.0161	0.0066	0.40	7.3	0.0055	42.9	0.00086	54.3	217	0.00008	0.052	653
204	0.061	0.00055	0.0016	0.026	0.0010	340	0.083	0.00025	110.1	31.0	0.0026	0.0044	0.0040	0.56	0.045	0.00012	30.3	0.056	0.0161	0.0066	0.40	7.3	0.0055	42.9	0.00086	54.3	217	0.00008	0.052	653
205	0.061	0.00055	0.0016	0.026	0.0010	340	0.083	0.00025	110.1	31.0	0.0026	0.0044	0.0041	0.56	0.045	0.00012	30.3	0.056	0.0161	0.0067	0.40	7.3	0.0055	42.9	0.00086	54.3	217	0.00008	0.052	653
206	0.061	0.00055	0.0016	0.026	0.0010	340	0.083	0.00025	110.1	31.0	0.0026	0.0045	0.0041	0.56	0.045	0.00012	30.3	0.056	0.0162	0.0067	0.40	7.3	0.0055	42.9	0.00086	54.3	217	0.00008	0.052	653
207	0.062	0.00055	0.0016	0.026	0.0010	340	0.083	0.00025	110.1	31.0	0.0026	0.0045	0.0041	0.56	0.045	0.00012	30.3	0.056	0.0162	0.0067	0.40	7.3	0.0055	42.9	0.00086	54.3	217	0.00009	0.052	653
208	0.062	0.00055	0.0016	0.026	0.0010	340	0.083	0.00025	110.2	31.0	0.0026	0.0045	0.0041	0.56	0.045	0.00012	30.3	0.056	0.0162	0.0067	0.40	7.3	0.0055	42.9	0.00086	54.3	217	0.00009	0.052	654
209	0.062	0.00055	0.0016	0.026	0.0010	340	0.083	0.00025	110.2	31.0	0.0026	0.0045	0.0041	0.56	0.045	0.00012	30.3	0.056	0.0162	0.0067	0.40	7.3	0.0055	42.9	0.00087	54.3	217	0.00009	0.053	654
210	0.062	0.00055	0.0016	0.026	0.0010	340	0.083	0.00025	110.2	31.0	0.0026	0.0045	0.0041	0.56	0.045	0.00012	30.3	0.056	0.0162	0.0067	0.40	7.3	0.0055	42.9	0.00087	54.3	217	0.00009	0.053	654
211	0.062	0.00055	0.0016	0.026	0.0010	340	0.083	0.00025	110.2	31.0	0.0026	0.0045	0.0041	0.56	0.045	0.00012	30.3	0.056	0.0162	0.0067	0.40	7.4	0.0055	42.9	0.00087	54.3	217	0.00009	0.053	654
212	0.062	0.00055	0.0016	0.026	0.0010	340	0.083	0.00025	110.2	31.0	0.0026	0.0045	0.0041	0.56	0.045	0.00012	30.3	0.056	0.0163	0.0067	0.40	7.4	0.0055	42.9	0.00087	54.3	217	0.00009	0.053	654
213	0.062	0.00055	0.0016	0.026	0.0010	340	0.083	0.00025	110.2	31.0	0.0026	0.0045	0.0041	0.56	0.045	0.00012	30.4	0.057	0.0163	0.0067	0.40	7.4	0.0055	42.9	0.00087	54.3	218	0.00009	0.053	654
214	0.062	0.00055	0.0016	0.026	0.0010	340	0.083	0.00025	110.2	31.0	0.0026	0.0045	0.0041	0.56	0.045	0.00012	30.4	0.057	0.0163	0.0067	0.40	7.4	0.0056	42.9	0.00087	54.3	218	0.00009	0.053	654
215	0.062	0.00055	0.0016	0.026	0.0010	340	0.083	0.00025	110.3	31.0	0.0026	0.0045	0.0041	0.56	0.045	0.00012	30.4	0.057	0.0163	0.0067	0.40	7.4	0.0056	42.9	0.00087	54.3	218	0.00009	0.053	654
216	0.062	0.00056	0.0016	0.026	0.0010	340	0.083	0.00025	110.3	31.0	0.0026	0.0045	0.0041	0.56	0.045	0.00012	30.4	0.057	0.0164	0.0067	0.40	7.4	0.0056	42.9	0.00087	54.3	218	0.00009	0.053	655
217	0.062	0.00056	0.0016	0.026	0.0010	340	0.083	0.00025	110.3	31.0	0.0026	0.0045	0.0041	0.56	0.045	0.00012	30.4	0.057	0.0164	0.0067	0.40	7.4	0.0056	42.9	0.00087	54.3	218	0.00009	0.053	655
218	0.062	0.00056	0.0016	0.026	0.0010	340	0.083	0.00026	110.3	31.0	0.0026	0.0045	0.0041	0.56	0.045	0.00012	30.4	0.057	0.0164	0.0067	0.40	7.4	0.0056	42.9	0.00087	54.3	218	0.00009	0.053	655
219	0.062	0.00056	0.0016	0.026	0.0010	340	0.083	0.00026	110.3	31.0	0.0026	0.0045	0.0041	0.56	0.045	0.00012	30.4	0.057	0.0164	0.0068	0.41	7.4	0.0056	42.9	0.00088	54.3	218	0.00009	0.053	655
220	0.062	0.00056	0.0016	0.026	0.0010	340	0.083	0.00026	110.3	31.0	0.0026	0.0045	0.0041	0.56	0.045	0.00012	30.4	0.057	0.0164	0.0068	0.41	7.4	0.0056	42.9	0.00088	54.3	218	0.00009	0.053	655
221	0.062	0.00056	0.0016	0.026	0.0010	340	0.083	0.00026	110.3	31.0	0.0026	0.0045	0.0041	0.56	0.045	0.00012	30.4	0.057	0.0164	0.0068	0.41	7.4	0.0056	42.9	0.00088	54.3	218	0.00009	0.053	655
222	0.062	0.00056	0.0016	0.026	0.0010	340	0.084	0.00026	110.4	31.0	0.0026	0.0045	0.0042	0.56	0.045	0.00012	30.5	0.057	0.0165	0.0068	0.41	7.4	0.0056	42.9	0.00088	54.3	218	0.00009	0.053	655

Table 9. Predicted Total Concentrations at Whitlow Ranch Dam - Alternative 4

Table 9. Predicted Total Concentrations at Whitlow Ranch Dam - Alternative 4

Years since Mine Start	Al	Sb	As	Ba	Be	HCO3	B	Cd	Ca	Cl	Cr	Co	Cu	F	Fe	Pb	Mg	Mn	Mo	Ni	NO3-N	K	Se	Si	Ag	Na	SO4	Tl	Zn	TDS
	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	
69	0.047	0.00064	0.0025	0.035	0.0010	342	0.062	0.00014	93.1	24.6	0.0018	0.0025	0.0034	0.42	0.048	0.00009	23.9	0.171	0.0084	0.0042	1.91	4.5	0.0025	37.4	0.00038	36.3	151	0.00005	0.0217	568
70	0.047	0.00064	0.0025	0.035	0.0010	342	0.062	0.00014	93.1	24.6	0.0018	0.0025	0.0034	0.42	0.048	0.00009	23.9	0.172	0.0084	0.0042	1.91	4.5	0.0025	37.4	0.00038	36.3	151	0.00005	0.0219	568
71	0.047	0.00064	0.0025	0.035	0.0010	342	0.062	0.00014	93.1	24.6	0.0018	0.0025	0.0034	0.42	0.048	0.00009	23.9	0.172	0.0084	0.0042	1.91	4.5	0.0025	37.4	0.00039	36.3	151	0.00005	0.0220	568
72	0.047	0.00064	0.0025	0.035	0.0010	342	0.062	0.00014	93.1	24.6	0.0018	0.0025	0.0034	0.42	0.048	0.00010	23.9	0.172	0.0084	0.0042	1.91	4.5	0.0026	37.4	0.00039	36.3	151	0.00005	0.0221	568
73	0.047	0.00064	0.0025	0.035	0.0010	342	0.062	0.00014	93.1	24.6	0.0018	0.0025	0.0034	0.42	0.048	0.00010	23.9	0.172	0.0085	0.0042	1.91	4.5	0.0026	37.4	0.00039	36.3	151	0.00005	0.0221	569
74	0.047	0.00064	0.0025	0.035	0.0010	342	0.062	0.00014	93.1	24.6	0.0018	0.0025	0.0034	0.42	0.048	0.00010	23.9	0.172	0.0085	0.0042	1.91	4.5	0.0026	37.4	0.00039	36.3	151	0.00005	0.0222	569
75	0.047	0.00065	0.0025	0.035	0.0010	342	0.062	0.00014	93.2	24.6	0.0018	0.0026	0.0034	0.42	0.048	0.00010	24.0	0.172	0.0085	0.0042	1.91	4.5	0.0026	37.4	0.00039	36.4	151	0.00005	0.0223	569
76	0.047	0.00065	0.0025	0.035	0.0010	342	0.062	0.00014	93.2	24.6	0.0018	0.0026	0.0034	0.42	0.048	0.00010	24.0	0.172	0.0085	0.0042	1.91	4.5	0.0026	37.4	0.00039	36.4	151	0.00005	0.0224	569
77	0.047	0.00065	0.0025	0.035	0.0010	342	0.062	0.00014	93.2	24.6	0.0018	0.0026	0.0034	0.42	0.048	0.00010	24.0	0.172	0.0086	0.0042	1.91	4.5	0.0026	37.4	0.00040	36.4	152	0.00005	0.0225	569
78	0.047	0.00065	0.0025	0.035	0.0010	342	0.062	0.00014	93.2	24.6	0.0018	0.0026	0.0034	0.42	0.048	0.00010	24.0	0.172	0.0086	0.0043	1.91	4.5	0.0026	37.4	0.00040	36.4	152	0.00005	0.0226	569
79	0.047	0.00065	0.0025	0.035	0.0010	342	0.062	0.00014	93.2	24.6	0.0018	0.0026	0.0034	0.42	0.048	0.00010	24.0	0.172	0.0086	0.0043	1.91	4.5	0.0026	37.4	0.00040	36.4	152	0.00005	0.0227	569
80	0.047	0.00065	0.0025	0.035	0.0010	342	0.062	0.00014	93.2	24.6	0.0018	0.0026	0.0034	0.42	0.048	0.00010	24.0	0.172	0.0086	0.0043	1.91	4.5	0.0026	37.4	0.00040	36.4	152	0.00005	0.0227	569
81	0.047	0.00065	0.0025	0.035	0.0010	342	0.062	0.00014	93.3	24.6	0.0018	0.0026	0.0035	0.42	0.048	0.00010	24.0	0.173	0.0087	0.0043	1.91	4.6	0.0026	37.4	0.00040	36.4	152	0.00005	0.0229	570
82	0.048	0.00065	0.0025	0.035	0.0010	342	0.062	0.00014	93.3	24.6	0.0018	0.0026	0.0035	0.42	0.048	0.00010	24.0	0.173	0.0087	0.0043	1.91	4.6	0.0026	37.4	0.00040	36.4	152	0.00005	0.0229	570
83	0.048	0.00065	0.0025	0.035	0.0010	342	0.062	0.00014	93.3	24.6	0.0018	0.0026	0.0035	0.42	0.048	0.00010	24.0	0.173	0.0087	0.0043	1.91	4.6	0.0026	37.4	0.00040	36.4	152	0.00005	0.0230	570
84	0.048	0.00065	0.0025	0.035	0.0010	342	0.062	0.00014	93.3	24.6	0.0018	0.0026	0.0035	0.42	0.048	0.00010	24.0	0.173	0.0087	0.0043	1.91	4.6	0.0027	37.4	0.00041	36.4	152	0.00005	0.0231	570
85	0.048	0.00065	0.0025	0.035	0.0010	342	0.062	0.00014	93.3	24.6	0.0018	0.0026	0.0035	0.42	0.048	0.00010	24.0	0.173	0.0087	0.0043	1.91	4.6	0.0027	37.4	0.00041	36.4	152	0.00005	0.0231	570
86	0.048	0.00065	0.0025	0.035	0.0010	342	0.062	0.00014	93.3	24.6	0.0018	0.0026	0.0035	0.42	0.048	0.00010	24.0	0.173	0.0088	0.0043	1.91	4.6	0.0027	37.4	0.00041	36.4	152	0.00005	0.0232	570
87	0.048	0.00065	0.0025	0.035	0.0010	342	0.063	0.00014	93.3	24.6	0.0018	0.0026	0.0035	0.42	0.048	0.00010	24.0	0.173	0.0088	0.0043	1.91	4.6	0.0027	37.4	0.00041	36.4	152	0.00005	0.0233	570
88	0.048	0.00065	0.0025	0.035	0.0010	342	0.063	0.00014	93.4	24.6	0.0018	0.0026	0.0035	0.42	0.048	0.00010	24.1	0.173	0.0088	0.0043	1.91	4.6	0.0027	37.4	0.00041	36.4	152	0.00005	0.0234	570
89	0.048	0.00065	0.0025	0.035	0.0010	342	0.063	0.00014	93.4	24.6	0.0018	0.0026	0.0035	0.42	0.048	0.00010	24.1	0.173	0.0088	0.0043	1.91	4.6	0.0027	37.4	0.00041	36.4	152	0.00006	0.0235	570
90	0.048	0.																												

Table 9. Predicted Total Concentrations at Whitlow Ranch Dam - Alternative 4

Table 9. Predicted Total Concentrations at Whitlow Ranch Dam - Alternative 4

Minimum	0.040	0.00052	0.0024	0.035	0.0010	342	0.057	0.00005	90.3	24.0	0.0015	0.0013	0.0023	0.41	0.048	0.00008	22.4	0.150	0.0030	0.0027	1.90	3.0	0.0007	37.4	0.00004	35.7	136	0.00003	0.0030	546
Maximum	0.052	0.00071	0.0025	0.035	0.0010	342	0.065	0.00017	95.1	24.7	0.0019	0.0031	0.0041	0.42	0.048	0.00011	24.9	0.178	0.0103	0.0049	1.91	5.1	0.0033	37.4	0.00049	36.5	161	0.00006	0.0293	582
Average	0.048	0.00065	0.0025	0.035	0.0010	342	0.062	0.00013	93.4	24.5	0.0018	0.0025	0.0035	0.42	0.048	0.00010	24.0	0.170	0.0082	0.0042	1.91	4.5	0.0025	37.4	0.00037	36.3	152	0.00005	0.0215	570

Surface

Digitized by srujanika@gmail.com

- Notes:**
^a Cd, Cu, Pb, Ni and Zn standards are hardness dependent and were calculated using lowest (most stringent) hardness value recorded for Whitlow Ranch Dam (307 mg/L CaCO₃ on 8/25/2017)
1. Constituent concentrations calculated by adding model results to median background constituent concentrations at Whitlow Ranch Dam
2. Surface WQ Standard = Arizona Department of Environmental Quality Water Quality Standard for "Aquatic and wildlife warm" (A&ww) water with chronic exposure (Arizona Administrative Code - Title 18, Ch. 11, Sup. 16-4, 2016)
3. Values in bold italic indicate that concentration is above water quality standard



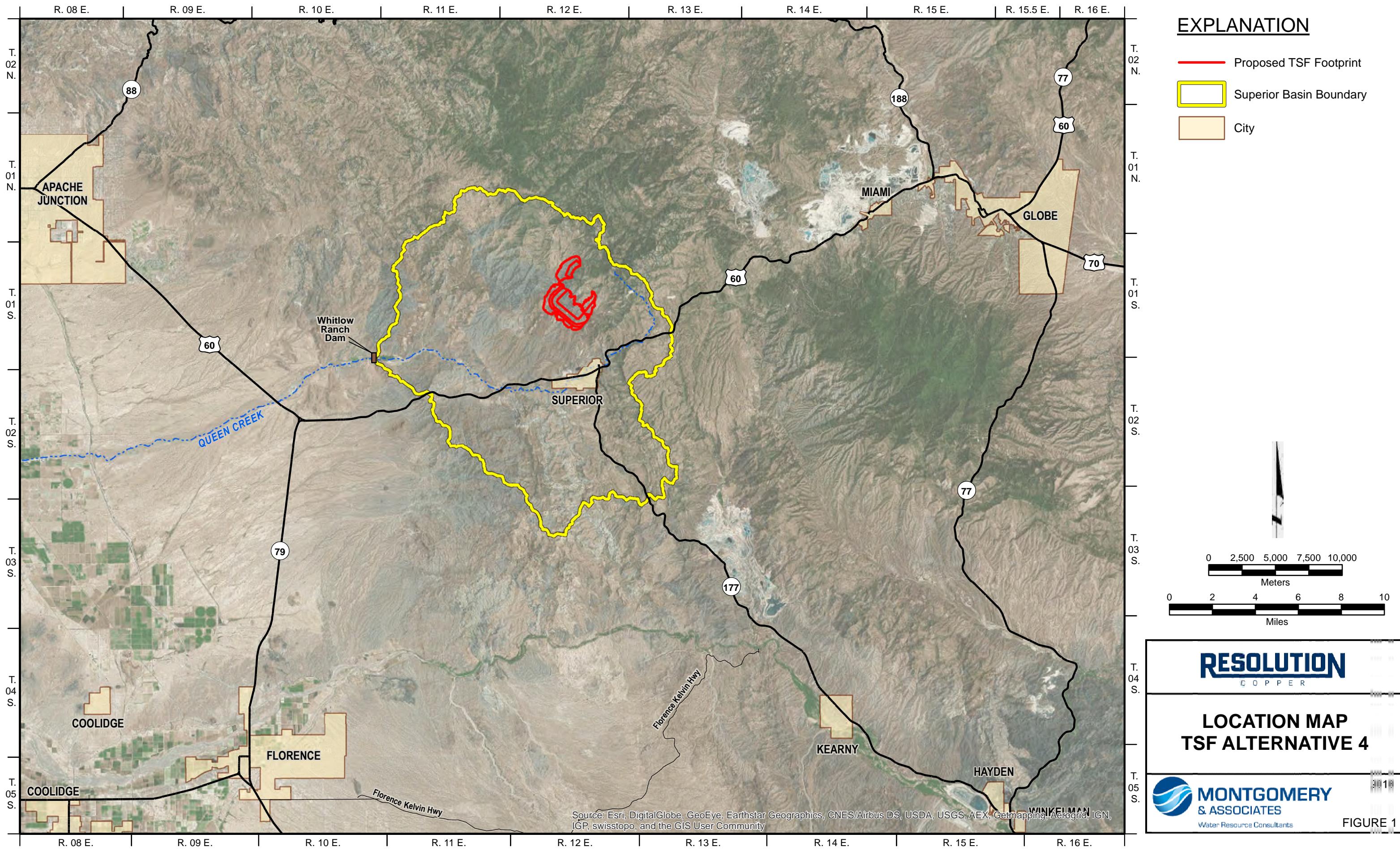
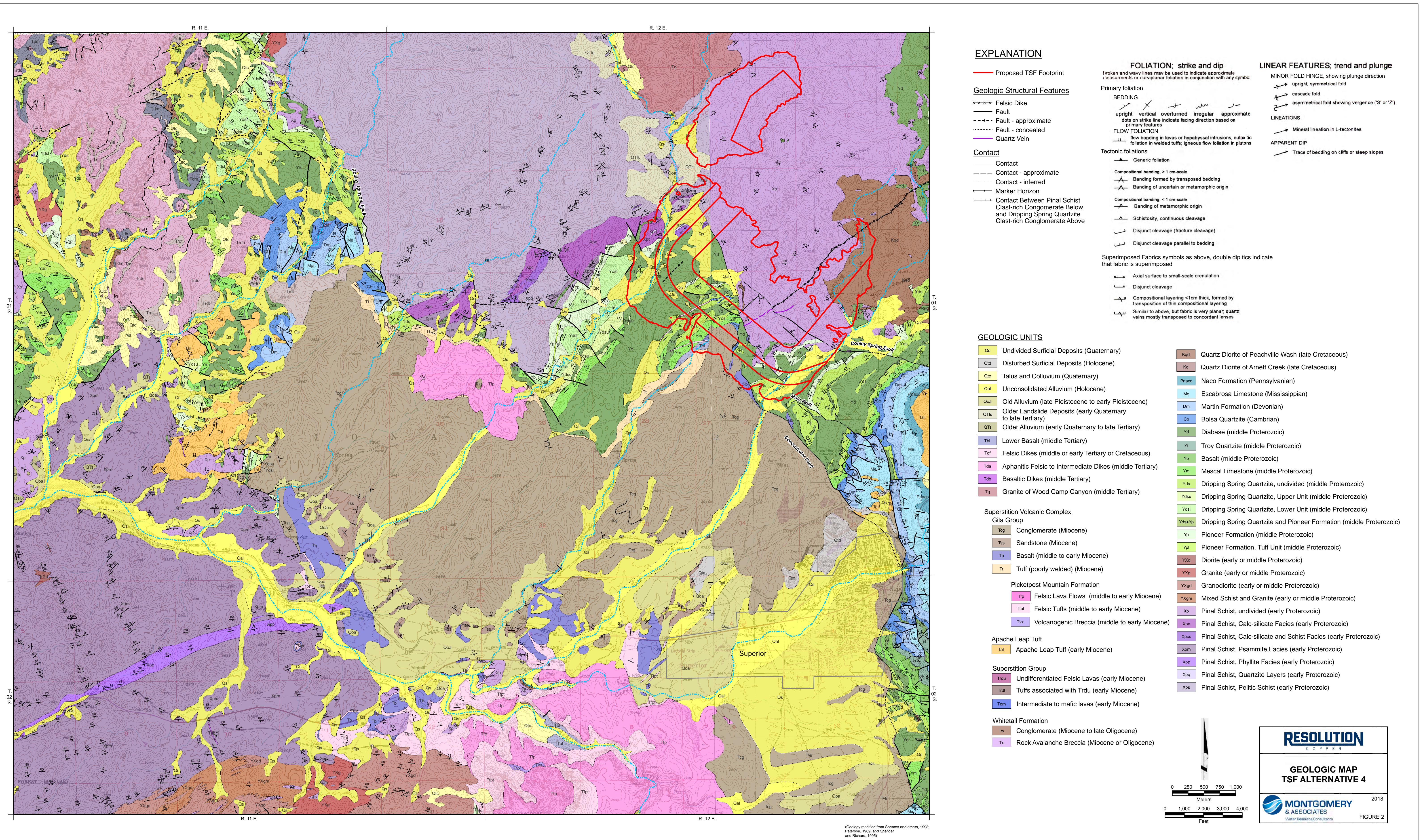
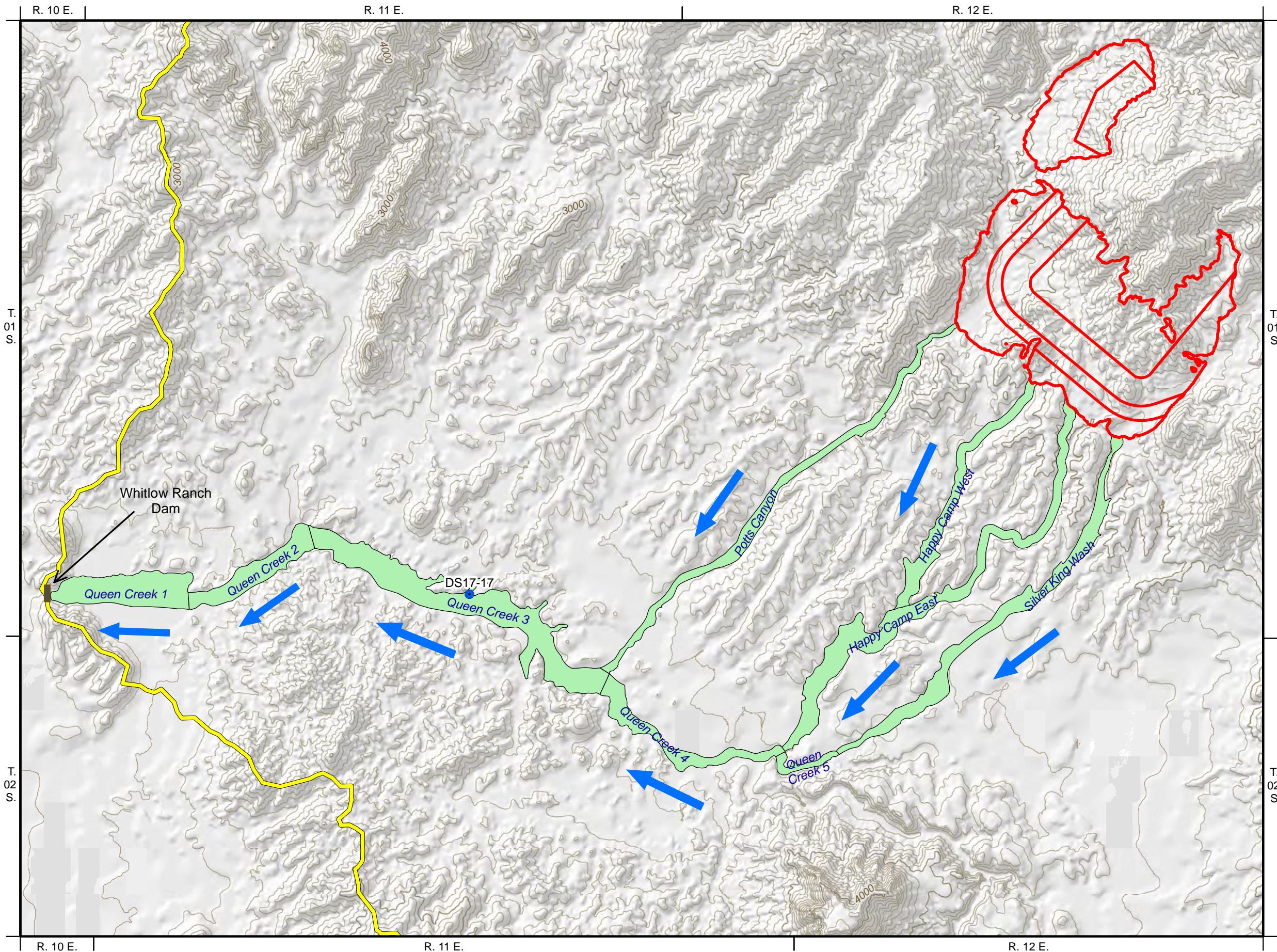


FIGURE 1





EXPLANATION

- Aquifer Subdomain
- Proposed TSF Footprint
- Superior Basin Boundary
- Flow Direction
- Well DS17-17

Aquifer Subdomain	Length (ft)	Area (ft ²)	Average Width (ft)
Silver King	20,100	10,219,800	510
Happy Camp E	23,700	14,186,100	600
Happy Camp W	12,300	6,052,900	490
Potts Canyon	23,400	8,340,600	360
Queen Creek 5	3,500	1,082,900	310
Queen Creek 4	9,900	5,398,500	550
Queen Creek 3	15,700	17,899,700	1,140
Queen Creek 2	6,400	5,656,700	880
Queen Creek 1	6,300	8,328,000	1,320

Notes:

1. Average widths of aquifer elements calculated by dividing aquifer polygon areas by lengths

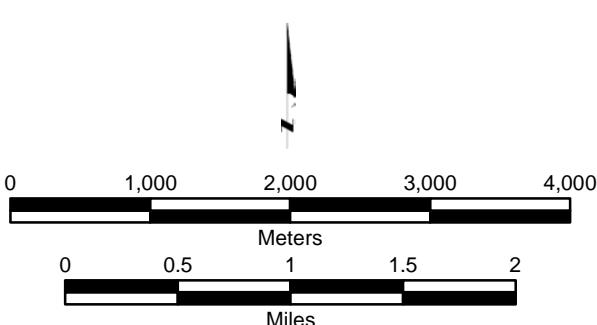


FIGURE 3



102 Magma Heights – P.O. Box 1944
Superior, AZ 85173
Tel.: 520.689.9374
Fax: 520.689.9304

September 17, 2018

Mr. Neil Bosworth
Supervisor – Tonto National Forest
US Forest Service
Supervisor's Office
2324 East McDowell Road
Phoenix, AZ 85006-2496

Subject: Response to ANALYSIS DATA REQUEST #1 – Request for Analysis of Tailings Seepage – Item #4 GoldSim Contaminant Transport Module.

Dear Mr. Bosworth,

To complete the response to item #4 from your March 8, 2018 letter, the following documents from Montgomery and Associates are enclosed:

- TSF Alternatives 2 and 3 – Near West: Life of Mine and Post-Closure Seepage Transport Modeling
- TSF Alternative 4 – Silver King: Life of Mine and Post-Closure Seepage Transport Modeling
- TSF Alternative 5 – Peg Leg: Life of Mine and Post-Closure Seepage Transport Modeling
- TSF Alternative 6 – Skunk Camp: Life of Mine and Post-Closure Seepage Transport Modeling

Sincerely,

A handwritten signature in blue ink that reads "Vicky Peacey".

Vicky Peacey,

Senior Manager, Environment, Permitting and Approvals; Resolution Copper Company, as Manager of Resolution Copper Mining, LLC

Cc: Ms. Mary Morissette; Senior Environmental Specialist; Resolution Copper Company



Enclosure(s):

Montgomery & Associates, September 2018. *TSF Alternatives 2 & 3 – Near West: Life of Mine and Post-Closure Seepage Transport Modeling.*

Montgomery & Associates, September 2018. *TSF Alternatives 4 – Silver King: Life of Mine and Post-Closure Seepage Transport Modeling.*

Montgomery & Associates, September 2018. *TSF Alternatives 5 – Peg Leg: Life of Mine and Post-Closure Seepage Transport Modeling.*

Montgomery & Associates, September 2018. *TSF Alternatives 6 – Near West: Life of Mine and Post-Closure Seepage Transport Modeling.*